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Environmental Characterization for the Sense and Destroy Armor (SADARM) Captive Flight Test, U.S. Army Yuma Proving Ground, Arizona, September 1990

by John O. Curtis, Flynn A. Clark Environmental Laboratory

> Frank E. Perron, Jr., John E. Fiori, Bryan G. Harrington, Stephen N. Decato Cold Regions Research and Engineering Laboratory



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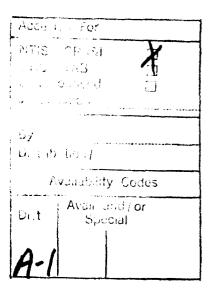
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> U.S. Army Corps of Engineers Waterways Experiment Station 3909 Halls Ferry Road Vicksburg, MS 39180-6199

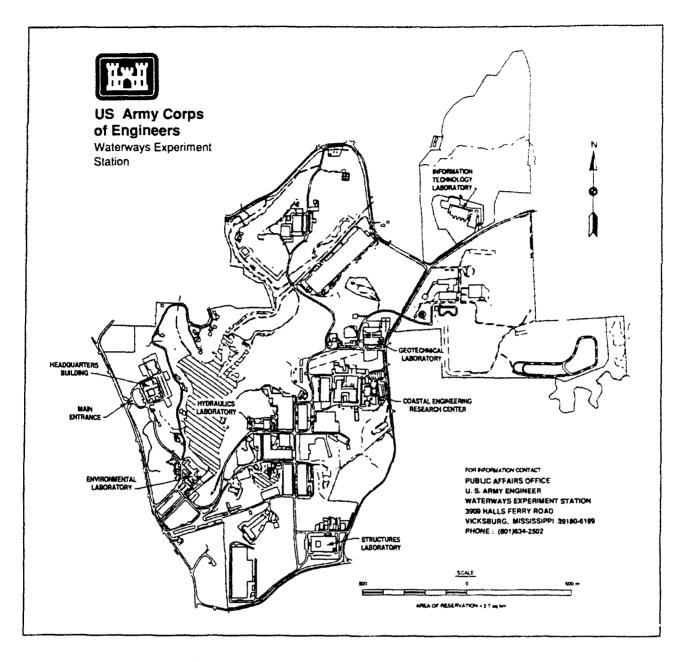
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Preface

The study reported herein was conducted by the U.S. Army Engineer Waterways Experiment Station (WES), Vicksburg, MS, and the Cold Regions Research and Engineering Laboratory (CRREL), Hanover, NH. It was funded by the U.S. Army Armament Research, Development and Engineering Center, Picatinny Arsenal, New Jersey.

This report was prepared by Dr. John O. Curtis, Mr. Flynn A. Clark, Environmental Systems Division (ESD), Environmental Laboratory (EL), WES, and Messrs. Frank E. Perron, Jr., John E. Fiori, Bryan G. Harrington, and Stephen N. Decato, Geophysical Sciences Branch, Research Division, CRREL. Data was collected by personnel from WES and CRREL. Dr. Curtis headed the WES field team, and Mr. Perron headed the CRREL team.

The study was conducted under the general supervision of Dr. John Harrison, Director, EL, and Dr. Victor E. LaGarde, Chief, ESD.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Leonard G. Hassell, EN. COL Palmer K. Bailey, CE, was Commander of CRREL, and Dr. Lewis E. Link was Director.

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1 Introduction

Background Information

The Army's Sense And Destroy Armor (SADARM) system is a parachute-delivered antiarmor weapon system currently undergoing full-scale engineering development. The final system configuration will consist of a submunition whose firing from some altitude above the target will be triggered by onboard algorithms whose input will include data from sensors that operate in both the thermal infrared and millimeter wave portions of the electromagnetic spectrum.¹

Prototype SADARM sensors have been tested under captive flight test conditions during various stages of their development by contractors competing for the production contract. The test program that took place at the U.S. Army Yuma Proving Ground (YPG) in September 1990 was one of a series of tests in desert environmental conditions. Overall SADARM system development responsibility lies within the Office of Project Manager, SADARM at the U.S. Army Armament Research, Development and Engineering Center (ARDEC), Picatinny Arsenal, New Jersey.

Objective of Study

ARDEC asked the U.S. Army Corps of Engineers to conduct test site measurements sufficient to characterize the background near targets within the sensors fields of view during the YPG captive flight tests. These data included measurements to determine the impact of changing environmental conditions (e.g., time of day, meteorology, immediate climatological history) on background signatures. This study provides data that is not only immediately useful to ARDEC and its contractors, but also to the long-term

Belcher, C. L., Richards, M. A., and Alexander, P. M. (1990). "Millimeter wave data reduction and analysis for support of system evaluation," Final Technical Report, Project A-8415, Georgia Institute of Technology, Atlanta, GA.

Corps of Engineers goal of developing and improving background signature models.

Scope of Report

Following an introductory section on how the site characterization data collection effort was conducted, subsequent sections of this report provide more detail on specific data sets; namely, what was measured, what instruments were used, and, where appropriate, data samples and/or the results of some preliminary analyses.

2 Data Collection Effort

Control Site

To avoid conflicts with activities within the actual SADARM test area, a nearby patch of terrain was selected for detailed characterization measurements (Figure 1). This area, hereafter referred to as the Control Site, was carefully chosen to be representative of the terrain contained within the SADARM test area, while at the same time being limited enough in extent to allow for meaningful terrain characterization measurements. The Control Site (Figure 2) contained most of the vegetation species that existed in the SADARM test area as well as a well-defined desert wash whose banks and gravel bottom could be easily viewed from the sensor platform described in the following paragraphs.

Observation Tower

A platform from which the Control Site could be viewed at various depression angles was designed and assembled (Figure 3). Sensors positioned on this platform included two thermal infrared imaging systems, an active millimeter wave radar, and two millimeter wave radiometers. Safety concerns limited the height of the observation tower to about 10 m. Further concerns about the possibility of sudden flooding through the wash because of heavy rains forced the tower to be placed far enough upslope from the wash banks to secure its footing.

Because of the safety factors discussed above, the resulting range of depression angles for viewing vegetation in the wash and other relevant wash features were limited to a range of 10 to 30 deg. While these angles are not typical of SADARM sensor parameters, they are nevertheless the best compromise available. Furthermore, the surrounding desert pavement could be viewed at depression angles of as much as 70 deg.

To convert degrees (angles) to radians, multiply by 0.1745329.

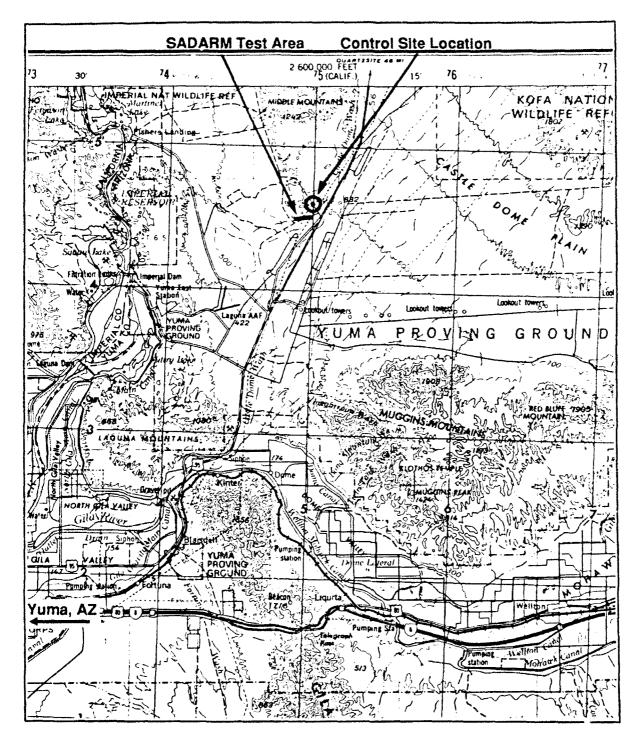


Figure 1. Control Site and SADARM test area locations

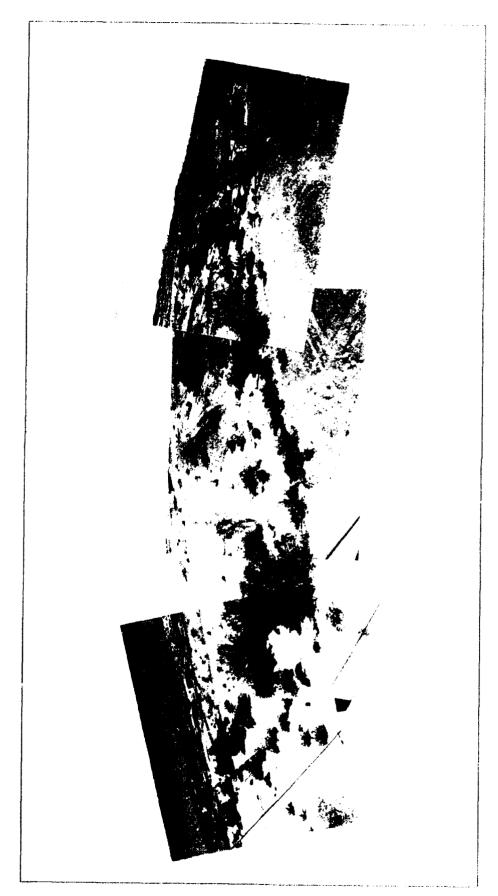


Figure 2. Photograph mosaic of the Control Site

A mobile measurement platform was discounted for two reasons. One was that such platforms are typically not stable enough to allow for the operation of the millimeter wave systems. Generally, one does not want more than a quarter of a wavelength of motion of a sensor during data collection. This allows only about 2 to 3 mm of motion during data collection, an unreasonable expectation for a mobile platform. Another reason for not using a mobile platform is that repeatability of data collection viewing angles and ranges to terrain patches is virtually impossible. One of the purposes of making these measurements is to examine the effects of varying environmental conditions on terrain electromagnetic signatures, and one must have confidence that sensor view angles are virtually unchanged over a range of measurement times.

An air-conditioned trailer was rented and placed adjacent to the observation tower to provide a facility for the array of computers and other system control hardware required for operation of the sensors on the tower and for the limited onsite analysis of those data as well as the meteorological data also collected near the Control Site. The trailer was unusable for its intended purposes for the first several days of onsite operations because of the unavailability of YPG personnel to complete the electrical power hookup.

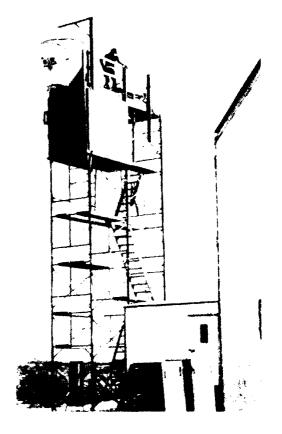


Figure 3. Observation tower and instrumentation trailer

Overview of Measurements

As stated earlier, the objective of this measurement exercise was to characterize the electromagnetic signatures of terrain in and near the SADARM test area that would form the background to targets being earched for by the contractor sensing systems during the Captive Flight Test. This involves not only image data or pseudo-image data that might be immediately useful to ARDEC and its contractors for establishing background signature statistics, but also data that can be used as input to first-principle terrain signature prediction models and data that simply provide a qualitative basis for what were the test site conditions.

Control Site measurements made during the SADARM Captive Flight Tests can be grouped into the following classes:

- a. Boundary layer radiation exchange data.
- b. Ground surface characteristics.

- c. Vegetation characteristics.
- d. Thermal infrared measurements.
- e. Active millimeter wave measurements.

Subsequent parts of this report will address each of the parameter measurements, describing in some detail the types of measurements, the frequency of data collection, the types of instruments used, and, in some cases, examples of preliminary data analyses.

3 Boundary Layer Radiation Exchange Data

Meteorological Information

During the early stages of setting up for measurements at the Control Site, personnel began collecting data that would provide input to atmo-

spheric boundary layer radiation exchange models as well as onsite weather reports. A 6-m meteorological tower (Figure 4) was set up near the observation tower and outfitted with instruments that recorded the following parameters:

- a. Air temperature and dew point at 0.5-, 2.0-, and 6.0-m elevations above the ground.
- b. Horizontal wind speed and wind direction at 0.5, 2.0, and 6.0 m.
- c. Barometric pressure at 1.0 m.
- d. Downwelling and upwelling radiation in the wavelength band of 0.3 to 50 μm at an elevation of 1.0 m.

A rain gauge was also set out near the met tower, but no precipitation occurred at the Control Site during the duration of these measurements. Data were collected from the met tower in 1-min intervals.

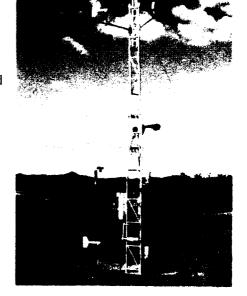


Figure 4. Control Site meteorological tower

Appendix A contains a complete listing of all of the meteorological measurements made at the Control Site, with each number representing an average of 1-min measurements made during the preceding 15-min period. Figure 5 is a plot of downwelling radiation over a period of several days combined with air temperature data at 0.5-m elevation that clearly shows that air temperature is not solely a function of solar loading. Over the 11-day period of data collection, peak daily solar loadings were comparable, while both mean and peak air temperature decreased with time.

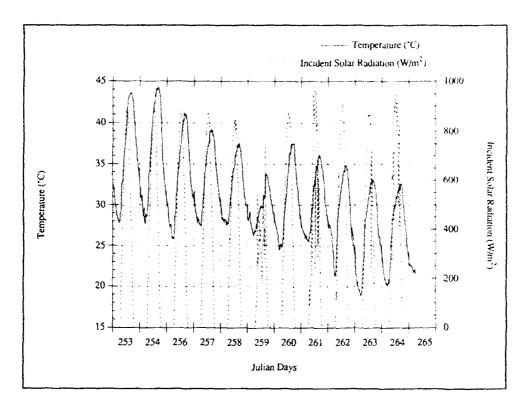


Figure 5. Diurnal variation of solar loading and air temperature

Soil Temperature Profiles

Two sets of near-soil-surface temperature profile data were collected within the Control Site. These data consisted of average physical temperatures measured by thermistors placed at known depths in soil pits and backfilled. Temperatures measured at 60-sec intervals were averaged over 15-min periods and recorded on magnetic tape using Campbell Scientific CR21 microloggers.

Two soil pits were dug for this purpose. One was located on the north side of the wash within the Control Site, and the other was located on the north bank of the wash (Figure 6). The soil outside of the wash was typically gravelly sand, while that on the bank consisted of a layer of about 40 cm of sandy silt overlaying gravelly sand. Thermistors were inserted into the soil in one corner of each pit at the approximate depths below the surface of 0.0, 2.5, 5.0, 10.0, 20.0, 40.0, and 70.0 cm. The thermistor wires leading to the microloggers were buried in a shallow trench from the profile location to where the microloggers were hidden from view of the sensors on the observation tower.

Appendix B contains a listing of the soil temperature profile data collected from each pit. Figure 7 is a plot of representative soil temperature data recorded in the wash bank pit. Note that the temperature at a 70-cm depth is stable and that gradients between the surface and 70 cm can be nearly +20 °C during the heat of the day and as much as -10 °C at night.



Figure 6. Soil pit being dug on the Control Site wash bank

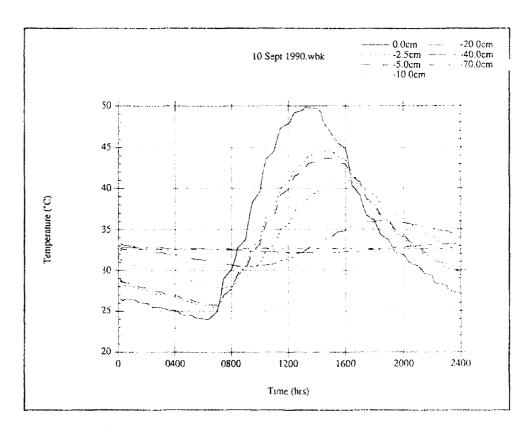


Figure 7. Representative wash bank soil temperature profiles

4 Ground Surface Physical Properties and Characteristics

General Description

Both the thermal infrared and active radar signatures of background terrain are dependent upon the material at the surface, the roughness of the surface at the appropriate sensor wavelength, and the geometry of the surface with respect to the sensor; i.e., surface slopes. General comments are in order prior to presentation of specific data.

Surface soil within both the SADARM test area and the Control Site can visually be classified into three broad categories. First of all there is the soil not affected by water flowing through the desert washes. It is typically a gravelly sand in which the gravel at the surface has been exposed by wind and water to form desert pavement (Figure 8), a layer of closely spaced small stones (most less than 2 cm) also subjected to chemical weathering to form the browish surface called desert varnish. As one moves closer to the wash, this desert pavement appears disturbed possibly by water action, the movement of animals, or by man. There is still a covering of surface stones, but without the desert varnish (Figure 9). It is the disturbed pavement that dominates the soil cover within the Control Site and near the washes within the SADARM test area.

The bottom of well-developed washes such as that within the Control Site typically contain a gravelly sand (Figure 10). Surface particle sizes are generally much smaller than those of the desert pavement. Hydrologic factors account for the deposition of this gravelly sand within the wash.

The banks of the wash are a complex mix of soil types. As indicated in an earlier section, a thick silt deposit exists high on the banks. Again, hydrologic factors could account for these deposits, with the lighter silt particles being dispersed throughout the flowing water rather than simply tumbling along the bottom of the wash as would be true for the gravel. It

is also possible, as shown in Figure 6, that the underlying material can also be exposed by water action, leaving a very rocky type of soil material.

Soil Classification

Appendix C contains the results of laboratory classification of various soil samples taken from the Control Site and reported in the nomenclature of the Unified Soil Classification System. Results labeled "Flat" refer to the samples taken from the soil pit dug in the gravelly sand outside of the wash, whereas those labeled "Wash Bank" refer to the pit dug in the bank of the wash.

Moisture Content

Moisture content in the test area soils can have a dramatic effect upon either the thermal infrared or millimeter wave signatures of the terrain background. Focusing again on the three types of surface soils, numerous soil moisture samples were collected during the conduct of this test site characterization effort. These samples were weighed onsite, sealed, and later dried and weighed again to determine gravimetric moisture contents. Figures 11-13 illustrate that the gravelly sands in both the wash bottom and outside of the washes were quite dry, as expected, with moisture contents varying between 0.75 and 2.5 percent.

Moisture content measurements on the sandy clayey silt on the wash banks were much more variable because of a combination of its texture and the prior weather at the test site. Several days prior to the arrival of the measurement team, the Yuma area had experienced heavy rains. As shown in Figure 6 by the darker patches of soil on the banks of the wash, some of the silt remained fairly wet for several days after the rain, probably because of the clay content of the soil. Data computed from samples taken in what apparently was damp soil are labeled as "wet" on Figure 13 and show a range of values from 13 to 17 percent. The "dry" wash bank silt moisture samples had values ranging from 1 to 4 percent, tending to be slightly higher in moisture content than the gravelly sands from the wash bottoms and surrounding areas.

Control Site Topography

Knowing what the ground elevations are like within the field of view may be very important, as well as the soil texture and moisture content, when interpreting the performance of a sensor that is scanning the terrain. Surface slope data are important in modeling the reflectance of all electromagnetic

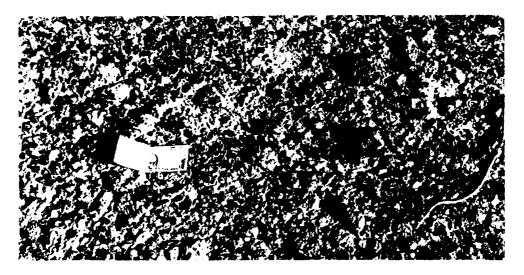


Figure 8. Typical desert pavement

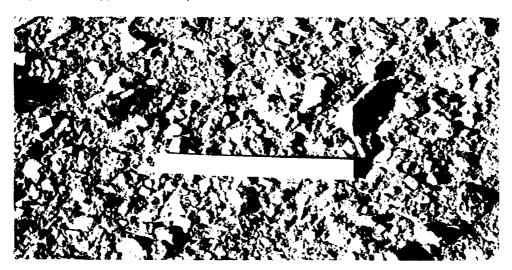


Figure 9. Disturbed desert pavement



Figure 10. Typical wash bottom material

energy, whether the energy source falls in the visible, thermal infrared, or millimeter wave portion of the spectrum. For this reason, a detailed topographic survey of the Control Site was conducted and the data included in the SADARM site characterization data package. Figure 14 is an example of these data plotted at a contour interval of 50 cm using the SURFER software package.

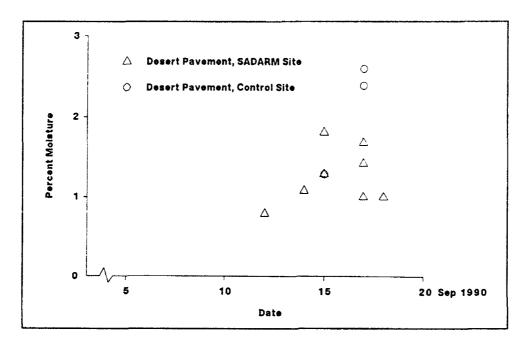


Figure 11. Gravimetric moisture contents for desert pavement

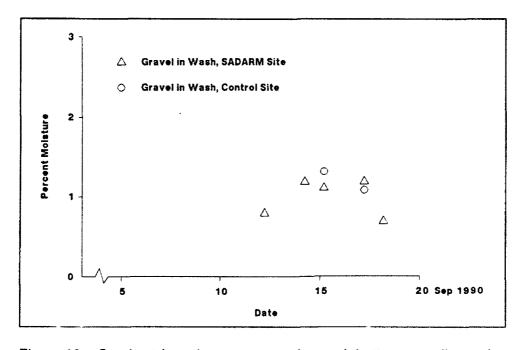


Figure 12. Gravimetric moisture contents for wash bottom gravelly sands

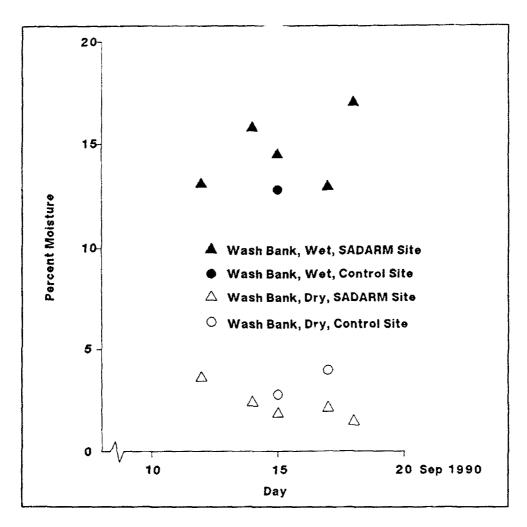


Figure 13. Gravimetric moisture contents for wash bank silt

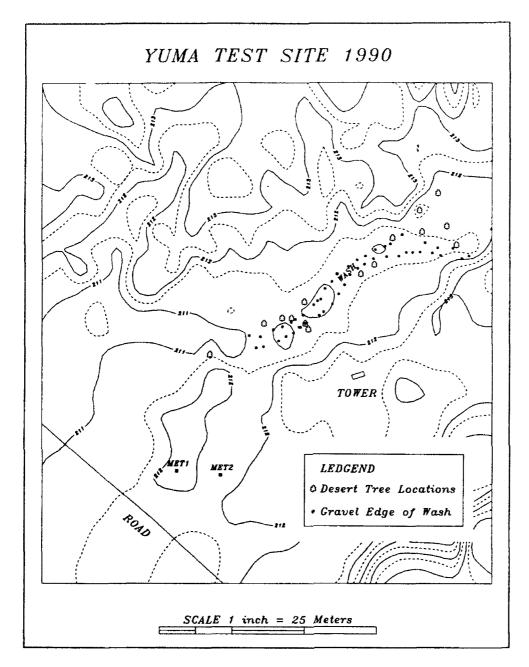


Figure 14. Control Site topography (50-cm intervals)

5 Vegetation Characteristics

General Description

Experience has shown that vegetation presents a definite thermal infrared contrast with background soil, especially during midday conditions of high solar loading. From an active millimeter wave sensor perspective, a large plant or tree serves as both a scattering center because of its wood structure and as an absorber because of its moisture content. In fact, living vegetation has often been modeled as a "cloud" of water, to a first approximation, because of the moisture contained within the twigs and leaves.

Most of the terrain at and near the SADARM test site and the Control Site has minimal vegetation cover. However, a significant amount of vegetation in the form of bushes and small trees exists along the banks of the desert washes, especially the well-developed washes. The following paragraphs describe the dominant species within this test area, provide quantitative data on surface area coverage, and discuss methods to estimate the volumetric moisture content of some of the species.

Table 1
SADARM Test Area and Control Site
Vegetation Species

Scientific Name	Common Name	Abbre- viation		
Ambrosia dumosa	white bur sage	AMDU		
Cercidium floridum	blue palo verde	CEFL		
Cercidium microphyllum	yellow palo verde	CEMI		
Encelia farinosa	brittlebush	ENFA		
Krameria paravifolia	white ratany	KRPA		
Larrea tridentata	creosote bush	LATR		
Lycium sp.	wolfberry	LY-		
Olyneya tesota	desert ironwood	OLTE		
Opuntia sp.	pencil cholla	OP-		
Note: sp = the species could not be identified in the field.				

Species Identification

Table I contains a list of the dominant species of vegetation that are found primarily in and around the developed washes at the SADARM test site and within the Control Site. Photographs of each of these species can be found in Appendix C.

Areal Densities

As indicated previously, desert pavement was nearly devoid of vegetation;

most plants and bushes were found within the well-developed wash areas Vegetation also existed in what were called "secondary washes" such as that shown in Figure 15, which are often not more than topographical depressions that collect water during rainfall. Quantitative data on the percent of ground cover offered by the various vegetation species were collected by selecting several vegetation sample sites within the SADARM test area and one site within the Control Site to facilitate the identification of different plant types and the calculation of ground cover or areal density from average plant diameter measurements. Table 2 identifies the physical area

included within each vegetation sample site, and Table 3 is a summary table for all areal density measurements. Note the extreme differences in percent cover between the desert pavement sample site and the three different developed wash sites.

Table 2 Vegetation Sample Site Areas				
Sample Site Name	Sample Site Location	Site Area m ²		
Desert Pavement	SADARM	3.684.1		
Secondary Wash	Test Site	408.5		
Developed Wash, Site 1		1,175 4		
Developed Wash, Site 2	<u> </u>	835.5		
Developeo Wash	Control Site	410.7		

The selection of the Control Site was considered representative of the developed wash

within the SADARM test area, since the total percent cover and individual species were approximately the same as in the test area.



Figure 15 Secondary wash sample site at the SADARM test area

			Sample 9	Site	
Species	Desert Pavement	Secondary Wash	Developed Wash, Site 1	Developed Wash, Site 2	Developed Wash Control Site
AMDU			_	American de la companya del la companya de la compa	0.75
CEFL	_			14.92	S works
CEMI	0.01		<0.01	4.30	**************************************
ENFA	0.22	0.40	5.73	4.25	5.65
KRGR	0.08			_	1.92
LATR	2.04	16.62	23.30	21.13	16.19
LY—		-	9.07	10.43	0.95
OLTE	_	3.39	18.04	15.60	28.46
UNK1		_	0.35	0.29	0.10
UNK2	_		1.16	1.22	Anapan Santa S
UNK3		_	0.31	0.43	
UNK4	_	I	0.91	0.48	
UNK5		_		0.04	
Totals	2.34	5.17	58.87	73.09	54.03

Moisture Content

Plant moisture content has a significant impact upon how much energy from the active millimeter wave sensor gets absorbed and/or scattered by the plant. Therefore, a limited number of plant-moisture measurements were conducted in the following way. A sample of leaves (if any), twigs, and branches for a selected plant was collected from a known volume within the plant. This sample was weighed onsite and later oven-dried and reweighed. From these measurements the average volumetric moisture content of several of the plant species was calculated and are shown in Table 4. Recent weather was expected to have a significant impact upon the number of samples taken for each species.

	Or Arciage	Plant Moisture C	untents	
Species	N	Plant Water	Plant, Dry	Water, percent
CEFL	5	865.48	774.82	53
CEMI	5	630.14	632.42	50
ENFA	7	851.00	1,057.55	45
LATR	5	449.50	824.94	35
LY—	4	646.63	1,875.35	26
OLTE	5	195.28	382.22	34

6 Thermal Infrared Measurements

In addition to characterizing the SADARM test site in terms of soil types, vegetation types, topography, and moisture contents, the measurement team also collected calibrated thermal infrared and active millimeter wave sensor data. This chapter of the report describes what kinds of thermal infrared data were collected.

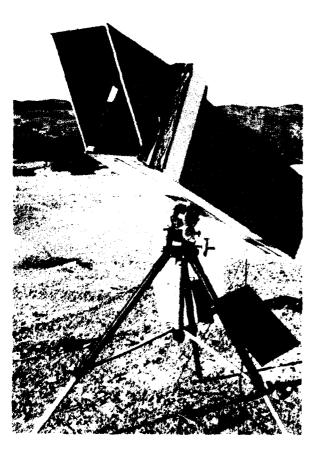


Figure 16. Ambient air temperature blackbody

Image Data

Measurement Setup

A pair of Inframetrics 500 thermal infrared imaging systems were attached to the frame of the observation tower at the Control Site on a remotely controlled panand-tilt unit placed about 9 m above the ground. One camera operated in the 3- to 5-µm wavelength band, while the other operated in the 8- to 12-µm band. Separate control units for each camera were operated within the air-conditioned tower enclosure immediately behind the cameras. Analog video images from each controller were recorded on separate VHS recorders. Both manual and audio logs were maintained for all scene recordings.

Calibration data for each set of imagery were collected by pointing the cameras at three different blackbodies located on the ground a few meters north of the observation tower. Figure 16 is a photograph of the ambient temperature blackbody. Figure 17 shows the two black plates used to



Figure 17. Two passive blackbody metal calibration plates

provide nonambient reference temperature values. All three devices were instrumented with thermocouples connected to a micrologger so that calibration device physical temperatures could be recorded at regular intervals.

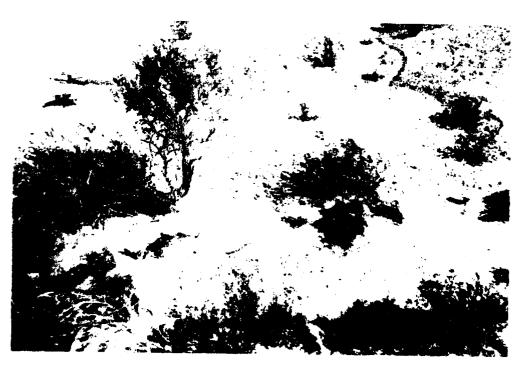
Summary of data collected

A list of all of the times and conditions under which thermal infrared imagery of the Control Site were collected is shown on Table 5. Each time data were collected, the measurement sequence included a scan of the blackbodies followed by a 10-sec scan at each of 11 predetermined views of the wash and its surroundings. Features of the scene were selected for image measurement based on experience and a preliminary scan of the terrain shortly after the observation tower was assembled and the imaging systems made operational. Photographs that approximate the fields of view of the thermal imaging systems for each of these predetermined views are included in Appendix D. As an example of the types of thermal imagery collected during this measurement period, Figure 18 contains images of one view of the Control Site wash taken at midnight, noon, and early evening that clearly show how environmental conditions can affect the background conditions. Given that white is hot in these thermal snapshots, one sees that the vegetation is hotter than the background at night, cooler than the surrounding soils at noon, and radiates thermal infrared energy at about the same rate as the soils during "crossover" periods that take place in the early evening (and early morning).

Table 5
Summary of Thermal Infrared Imagery

Date	Time, hr	3 to 5 μm	8 to 12 μm	Remarks
13 Sep 90	0730-0749	x		8- to 12-μm infrared system
	0830-0844	x		experiencing phasing problems
	1106-1119	x		
	1231-1242	X		
	1407-1413	x		
	1459-1508	X		
14 Sep 90	0759-0804	×		
	0902-0909	×		
	1013-1020	X		
	1102-1108	X		
	1154-1200	X		
··	1259-1305	X		
15 Sep 90	0032-0036	×	x	Start of diurnal test
	0100-0105	X	X	Many high winds
	0151-0154	X	X	Very high winds
	0212-0217	X	X	
	0309-0315 0400-0405	X	X X	
	0500-0506	×	X	}
	0600-0606	×	x	
	0700-0705	×	Î	
	0838-0843	x	Î	•
	0900-0905	x	x	
	0915-0919	x	x	
	1200-1205	x	x	
	1412-1417	×	x	
	1500-1505	x	x	•
	1603-1608	x	x	
	1730-1737	x	×	}
	1800-1805	x	x	· ·
	1811-1815	×	×	
	1900-1905	×	X	
	2018-2022	X	X	
	2124-2129	X	×	
	2200-2204	x	X	
	2300-2305	X	×	
	2345-2350	X	X	
17 Sep 90	0800-0816	×	×	
	0830-0834	X	X	
	0900-0904	X	X	
	1010-1014] ×	X	
	1100-1112	X	X	
	1208-1211 1320-1324	X	X	
	1403-1407	X	X X	
	1453-1457	×	x	
	1501-1504	×	x	
18 Sep 90	1250-1253	×	×	Site of 1st experiment
in ach an	1300-1311	x	×	One of 15t experiment
	1315-1316	×	X	
	1330-1331	x	x̂	
	1344-1346	x	x	1
	1404-1405	x	x	
	1415-1416	Î	x	
	1447-1448	x	x	
	1501-1501	x	x	
	1502-1502	×	×	}
		ı	l l	1
	1528-1528	X	X	1

Date	Time, hr	3 to 5 μm	8 to 12 μm	Remarks
19 Sep 90	0748-0748	X	X	Control scene only
·	0957-0958	X	x	Control scene only
	1001-1001	Ìχ	X	
	1003-1006	x	x	į.
	1008-1011	x	X	
	1142-1143	x	x	
	1323-1324	x	X	
	1503-1504	x	x	
	1521-1521	x	x	Site of 2nd experiment
	1523-1523	x	×	Site of 2nd experiment
	1558-1558	x	x	Water added
20 Sep 90	0813-0819	×	x	
•	0917-0922	x	x	
	1022-1027	x	x	
	1308-1314	x	x	



a. Visual

Figure 18. Control Site, scene 4 imagery (Continued)

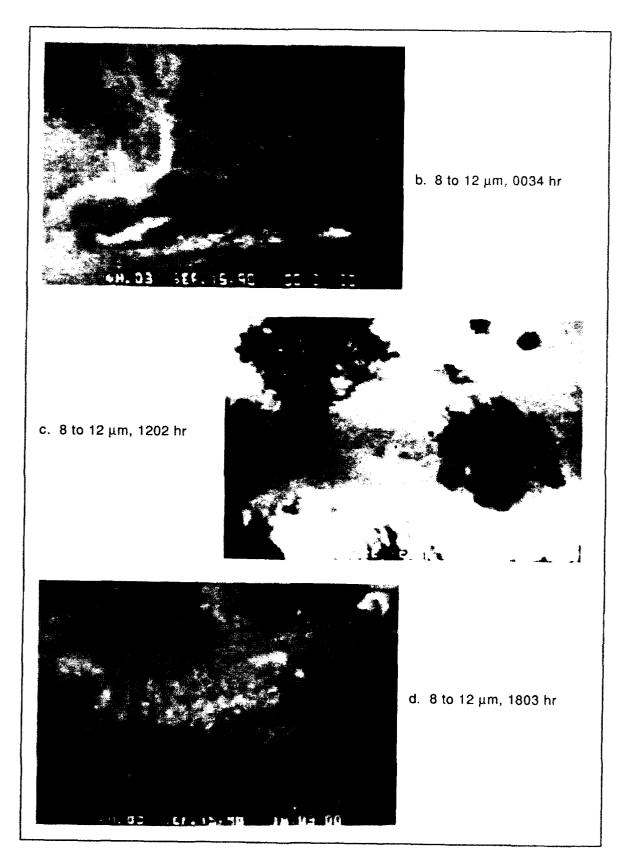


Figure 18. (Concluded)

Additional Measurements

Measurement setup

In an effort to quantify the temporal behavior of the thermal infrared signature of terrain within the Control Site (and, hence, the SADARM test area), a small portion of the wash that was out of view of the millimeter wave systems was selected for further measurements. At this location (Figure 19), eight staring radiometers, operating in the 8- to 14-µm band of wavelengths, were positioned on support poles to acquire data on selected terrain features listed in Table 6. Photographs that indicate what was being viewed by each radiometer are contained in Appendix E.

Table 6 Terrain Features Examined by the Staring Radiometers				
Radiometer Number Terrain Feature				
1	Undisturbed desert pavement			
2	Vegetation (AMDU), south side			
3	Wash gravel			
4	Shaded bank soil			
5	Wash bank, north-facing			
6	Vegetation (ENFA), south side			
7	Vegetation (??), west side, later pointed toward silty soil			
8	Deadwood, south side			

Summary of data collected

One-minute average temperatures for each of these radiometers were stored on a Campbell Scientific 21X micrologger. Appendix D contains the tabulated results of those measurements. Because of problems with the holding mechanism, results for Radiometer 7 are not considered valid until 1715 hr on Day 263, at which time the radiometer was pointed downward toward the silt on the wash bank and the holder firmly tightened. As an example of the kind of data available from these measurements, Figure 20 shows the temporal variation in wash gravel apparent temperatures over a period of several days.



Figure 19. Photograph of the spot temperature measurement site

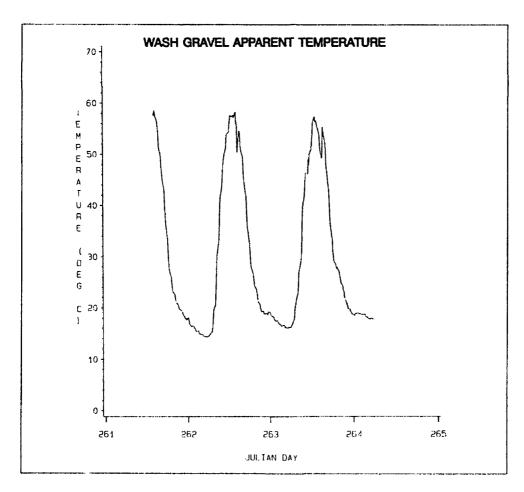


Figure 20. Temporal variation in radiometric temperature for wash gravel

Simulated Rainfall Experiments

Because of the total absence of rainfall during the Captive Flight Tests, two simulated rainfall experiments were conducted near the end of the measurement period. The purpose of these experiments was to demonstrate the dramatic change in terrain thermal infrared signatures caused by high soil moisture levels and to obtain quantitative data on how quickly the terrain surface can dry out following a significant rainfall event.

The first experiment was conducted on the gravelly, clayey, silty, sand near the base of the observation tower. The view through the thermal infrared cameras was at a depression angle of about 40 deg. An area on the ground of about 5 m² was wetted with enough tap water to approximate a rainfall of about 1 cm. Soil moisture samples were collected periodically, the results of which are shown in Table 7. Thermal infrared images of the wet soil and its immediate surroundings were collected during the times listed in Table 5. A preliminary review of the image data indicates that the initial thermal contrast between the wet soil and its surroundings was approximately 6 °C. The soil surface took about 2 days to dry out.

A second experiment was conducted on the sandy, clayey, silt on the south bank of the wash in front of the observation tower. The resulting depression angle for the thermal imaging cameras was about 25 deg. As before, soil moisture samples were collected and image data collected. Initial thermal contrast was approximately 6 to 7 °C, and, as with the gravelly sand, the silt took about 2 days to return to the dry state.

Table 7
Soil Moisture Measurements Supporting the Simulated Rainfall Experiments

Soil	Date	Time hr	Moisture Content percent	Note		
Gravelly sand	9/18/90	1230	0.7	Background		
	9/18/90	1240	12.8	Immediately after wetting		
	9/18/90	1310	12.5	Wet soil		
	9/18/90	1345	10.7	Wet soil		
	9/18/90	1415	9.9	Wet soil		
	9/18/90	1445	8.6	Wet soil		
	9/18/90	1545	7.4	Wet soil		
	9/19/90	0845	1.2	Background		
	9/19/90	0849	4.3	Wet soil		
	9/20/90	0750	2.4	Wet soil		
	9/20/90	0810	2.1	Background		
Sandy silt	9/19/90	1550	1.8	Background		
	9/19/90	1600	34.2	Immediately after wetting		
	9/19/90	1630	24.2	Wet soil		
	9/19/90	1700	23.6	Wet soil		
	9/19/90	1730	22.2	Wet soil		
	9/20/90	0758	14.8	Wet soil		
	9/20/90	1730	2.7	Wet soil		

7 Active Millimeter Wave Radar Measurements

Measurement Procedure

Another part of the ground truth electromagnetic signature data set was that collected by the active K_a -band scatterometer located at the top of the Control Site observation tower. The scatterometer (shown in Figures 21 and 22) was operated remotely from the trailer parked at the base of the tower. Because of the adverse temperature and dust conditions that existed at the Control Site, care was taken to protect the scatterometer components by enclosing the pan-and-tilt unit in a reflective blanket that allowed freedom of movement and by covering the transmitter and receiver boxes with reflective materials wherever possible. Air-conditioning was provided by blowing air from the thermal infrared control room on the tower up into the protective blanket. Holes in the base of the transmitter and receiver boxes allowed some of that air to be passed through to their delicate components.

The scatterometer is controlled by a Hewlett Packard 8510B Network Analyzer System. As configured for the YPG measurements, a signal covering the bandwidth of 2.0 to 2.5 GHz in 400 increments was sent to the transmitter front end via semirigid coaxial cable where it was upconverted to a sweep of 33.0 to 33.5 GHz. This results in a theoretical range resolution of 30 cm. The 400 frequency increments mean that the alias-free range is 240 m, which was more than enough to cover the terrain being measured. This scatterometer was configured to transmit horizontal and vertical polarizations and to receive both polarizations. It is capable of transmitting and receiving circular polarizations, but this feature has not been tested.

External calibration measurements were facilitated by placing two different aluminum corner reflectors on camera tripods at a range of about

¹ Zoll, M. (1990). "Design and construction of a K_a-band scatterometer," Draft Report, U.S. Army Ballistic Research Laboratory, Aberdeen Proving Ground, MD.

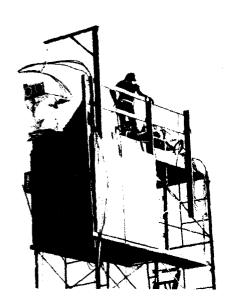


Figure 21. The K_a-band scatterometer on top of the observation tower



Figure 22. Close-up view of the scatterometer

22 m from the antennas. One reflector was a trihedral having a theoretical radar cross section of 9.39 dBsm, while the other was a dihedral with a theoretical cross section of 8.344 dBsm. The tripods were not covered. The trihedral was tilted up toward the antennas and its position adjusted to give the strongest received signal in the like-polarization channels. The dihedral was manually positioned at an angle of 45 deg to give the strongest signal in the cross-polarization channels.

The spatial pattern of measurements conducted with the scatterometer can best be visualized by referring to Figure 2. The tribedral and dihedral corner reflectors were placed on tripods positioned to the left of the oberservation tower. The trihedral can be seen at the lower left-hand corner of Figure 2. Beginning with the transmitter polarization set to vertical, the trihedral was illuminated, followed by the dihedral. A scan of the desert pavement (out of view to the left in Figure 2) was then conducted in 2-deg depression angle increments, beginning with 30 deg and ending at 70 deg. Two-degree increments were chosen to provide overlapping data; the antennas have circular radiation patterns with 4.1-deg beamwidths. The antennas were then pointed at a terrain feature in the wash at the far righthand side of Figure 2, and a scan pattern was begun to the left that covered an azimuth sweep of 80 deg in 2-deg increments and 11 scans from a starting depression angle of 10 deg to a final angle of 30 deg. This scan pattern covered all of the significant vegetation and wash bank features visible in Figure 2. Following completion of the wash scan, three additional azimuth

sweeps (at depression angles of 40, 50, and 60 deg) of the bare desert soil in front of the observation tower were conducted. The antennas were then pointed again at the trihedral, the transmitter polarization—as changed to horizontal, and the process repeated. Finally, the antennas were pointed at the sky and measurements made to help quantify the noise floor. This scan pattern is sketched in Figure 23.

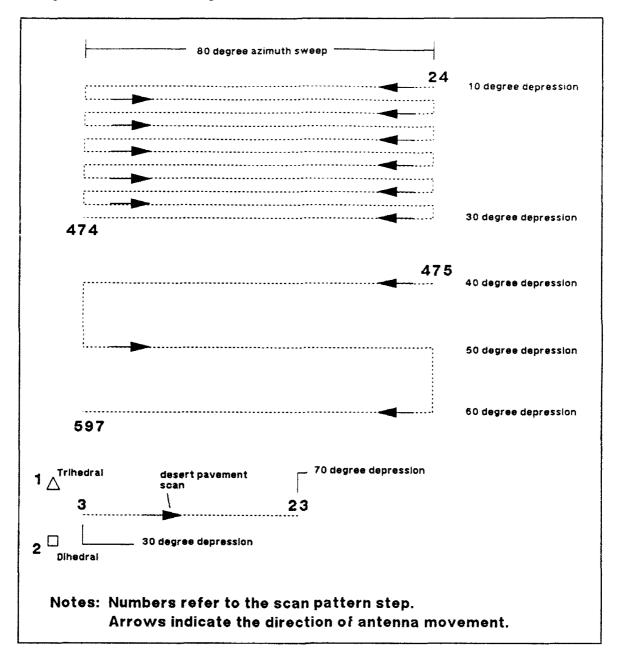


Figure 23. Scatterometer scan pattern

The entire measurement procedure was relatively slow as compared with the response time of tactical radar systems. The primary reason for this is because the network analyzer used to control the scatterometer is a

scientific data collection device designed for accuracy and stability, but not the speed of operation demanded by tactical systems. Each complete measurement sequence took about 1 hr and 50 min.

Measurements of the wetted soils were also made so that later analyses might reveal the effects of water on millimeter wave backscatter from moist soils as compared with dry soils. Table 8 contains a listing of the scatterometer data that was collected at YPG.

Table 8 Summary of	Scatterometer Date	a Collected at YPG
Date	Start Time, hr	Description
9/13/90	0304	Full Control Site scan
9/14/90	0529	Full Control Site scan
9/14/90	1818	Full Control Site scan
9/14/90	2306	Full Control Site scan
9/15/90	0420	Full Control Site scan (vertical transmit only)
9/15/90	0534	Full Control Site scan
9/15/90	1137	Full Control Site scan
9/15/90	1836	Full Control Site scan
9/17/90	1244	Full Control Site scan
9/18/90	1244	Wet gravel measurements
9/18/90	1314	Wet gravel measurements
9/18/90	1345	Wet gravel measurements
9/18/90	1417	Wet gravel measurements
9/18/90	1445	Wet gravel measurements
9/18/90	1545	Wet gravel measurements
9/19/90	1540	Wet silt measurements
9/19/90	1600	Wet silt measurements
9/19/90	1632	Wet silt measurements
3/19/90	1702	Wet silt measurements
9/19/90	1731	Wet silt measurements
9/20/90	0741	Wet silt measurements
9/20/90	1000	Wet silt measurements
9/20/90	1136	Wet silt measurements
9/20/90	1517	Wet silt measurements
9/20/90	1718	Wet silt measurements
9/20/90	1537	Wet gravel measurements (2nd time)
9/20/90	1555	Wet gravel measurements (2nd time)
9/20/90	1605	Wet gravel measurements (2nd time)
9/20/90	1634	Wet gravel measurements (2nd time)
9/20/90	1723	Wet gravel measurements (2nd time)

Preliminary Data Analysis

Radar cross-section measurements

Some preliminary analyses have been conducted and are described in the next few paragraphs. These studies were performed on the same Hewlett Packard 9000 Series 300 computer that was used to control the network analyzer during the field measurements.

The first analysis is one designed to produce a radar cross-section (RCS) map of the Control Site study area. Such a map gives an indication of where the strongest scattering centers are located within the field of view. The maximum RCS value for each range resolution cell at a given azimuth position was determined by systematically tabulating returns for every measurement made during the measurement sequence. The simplified radar range equation was used to perform these calculations under the assumption that all quantities are constant within the range resolution cell being considered. Normalized radar cross-section calculations of the vegetation cover and rough terrain within the Control Site wash are impossible because illuminated area cannot be determined. A flat earth assumption is meaningless for this site.

A representative RCS map for a vertical transmit, vertical receive scatterometer configuration is shown in Figure 24. Without much imagination, one can see the 40-, 50-, and 60-deg desert soil scans at the base of the fan. Other strong returns appear to be associated with some of the vegetation and sharp terrain features that could cause enhanced backscatter. While it is possible to refer to the photomosaic in Figure 2 as an aid in interpreting the returns shown on the RCS map, a one-to-one correspondence with terrain features is still not possible until the RCS data are combined with a three-dimensional topographic map to ascertain what is being illuminated by the scatterometer at each range and azimuth. The strip to the left of the main fan in Figure 24 is the desert pavement scan that is conducted first in each measurement sequence.

Normalized radar cross sections of desert pavement

A separate analysis was performed on the desert pavement data; i.e, those data collected at the beginning of each scan that cover depression angles ranging from 30 to 70 deg. Because the terrain at this location is almost flat, it is possible to make some assumptions about illuminated area and compute a normalized radar cross section, or backscatter coefficient, often referred to in the literature as σ . Again, the simplified radar range equation was utilized with the assumption that all quantities were constants within the half-power (or 3 dB) beamwidth. That beamwidth was used to calculate an illuminated area. Table 9 contains a list of these calculations for each depression angle of the scatterometer. Range is the slant range, in meters, to the peak return from the terrain surface. RCS is in units of

dBsm (dB above a square meter), area is in square meters, and the back-scatter coefficient is in dB. An average coefficient was computed from the nonlogarithmic values.

Table 9 Represent	ative Backsc	atter Coeffici	ent Calculatio	ns
Angle	Range	RCS	Area	σ
30.0	24.2	-7.8	0.600	-5.6
32.0	21.8	-9.8	0.551	-7.2
34.0	21.2	-6.2	0.549	-3.6
36.0	20.4	-6.7	0.542	-4.0
38.0	20.4	-11.2	0.557	-8.7
40.0	18.4	-12.3	0.515	-9.4
42.0	18.2	-11.8	0.525	-9.1
44.0	17.3	-9.3	0.515	-6.4
46.0	17.1	-9.4	0.527	-6.6
48.0	16.9	-15.2	0.541	-12.6
50.0	15.8	-11,1	0.526	-8.3
52.0	15.9	-13.9	0.556	-11.3
54.0	15.4	-14.2	0.562	-11.7
56.0	14.8	-11.4	0.569	-9.0
58.0	14.6	-8.3	0.592	-6.1
60.0	14.2	-9.2	0.612	-7.1
62.0	13.7	-11.7	0.626	-9.7
64.0	13.7	-8.7	0.670	-7.0
66.0	13.1	-14.0	0.693	-12.4
68.0	13.1	-14.6	0.752	-13.3
70.0	12.9	-10.6	0.812	-9.7
Average Backs	catter Coefficient =	-7.71 dB.		

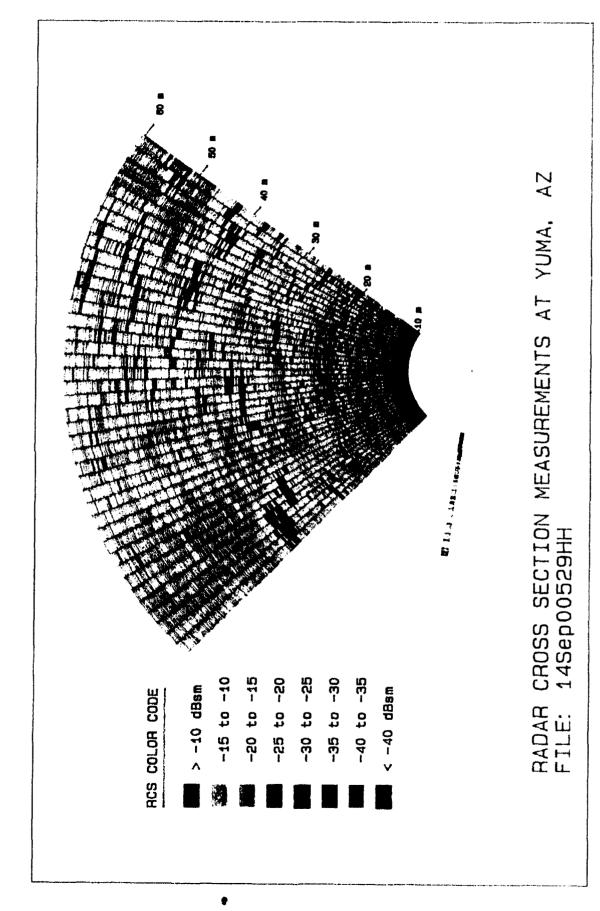


Figure 24. Representative RCS map of the Control Site

Appendix A Meteorological Data

The following pages list weather parameter data and other data useful for evaluating the atmospheric boundary layer energy exchange phenomenon at the Control Site near the Serve and Destroy Armor test area, Yuma Proving Ground, AZ. These data were collected during a 2-week period in September 1990. Tabulated data represent 15-min averages. Parameter definitions are as follows:

TIME hhmm local standard time in 24-hr format

PRESS mbs pressure in millibars

TEMP c temperature in degrees Centigrade

RH % relative humidity in percent
WD/SP mph wind speed in miles per hour

WD/DIR dir wind direction in degrees relative to true north
PRCP mm precipitation in millimeters (water equivalent)

VSBY km visibility in kilometers

PSP vert radiation flux in watts/m², 0.3- to 3-µm sensitivity

pyranometer facing up

PSP invert radiation flux in watts/m², 0.3- to 3-µm sensitivity

pyranometer facing down

PIR vert radiation flux in watts/m², 3- to 50-µm sensitivity

pyrgeometer facing up

PIR invert radiation flux in watts/m², 3- to 50-µm sensitivity

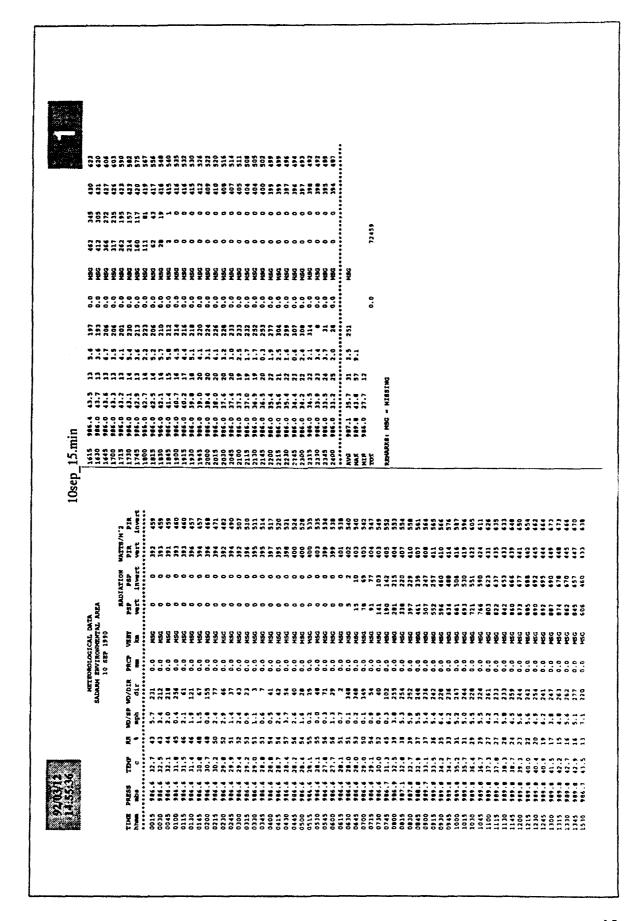
pyrgeometer facing down

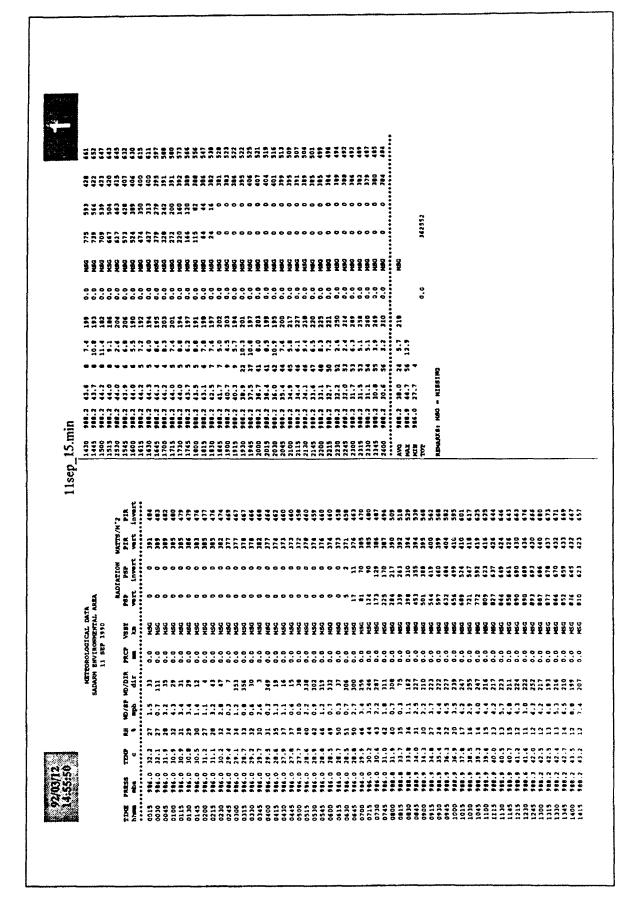
Tabulated data are followed by diurnal plots of several of the parameters. Solar radiation plots are taken from the pyranometer data, while long-wave radiation plots represent pyrgeometer measurements.

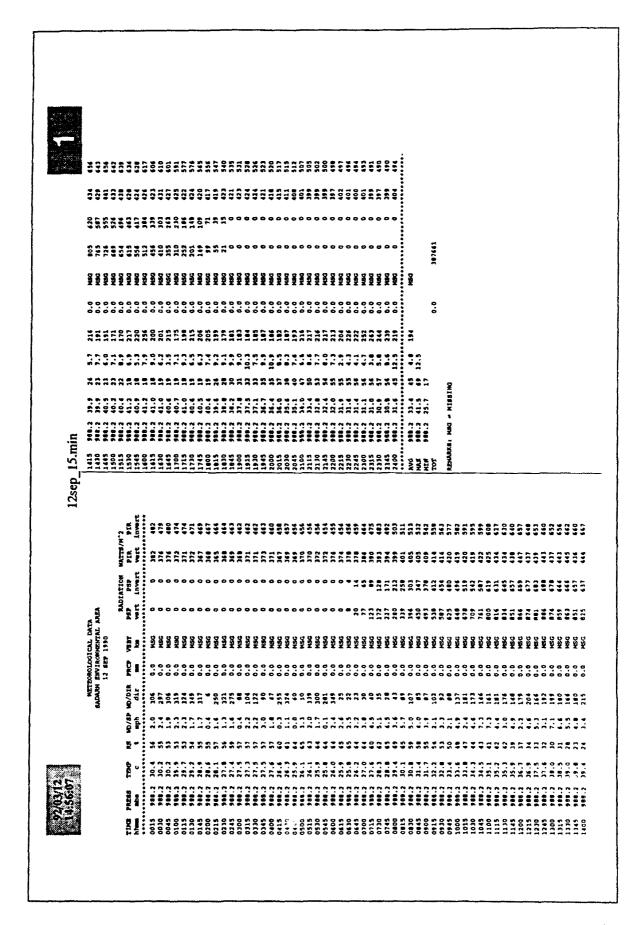
In addition to the data listed in this report, other information is available from the data files stored at the Cold Regions Research and Engineering Laboratory, including daily weather observations taken by the U.S. Army

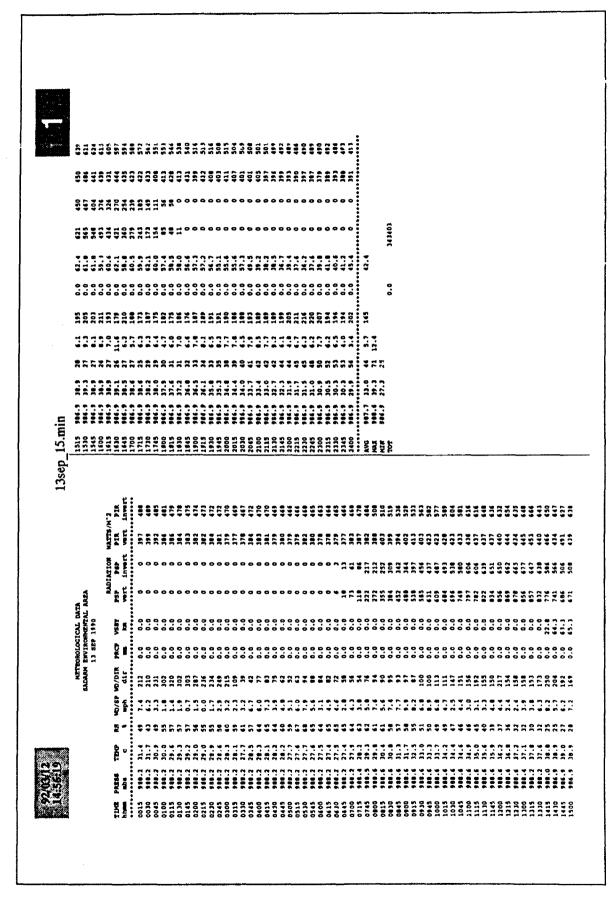
Atmospheric Sciences Laboratory (ASL), Yuma meteorological team, daily synoptic RAWINSONDE (balloon-borne instrument for measuring air temperature, humidity, presure, and wind speed) upper air soundings also provided by the ASL met team, and a climatological summary for the Yuma Proving Grounds for the month of September.

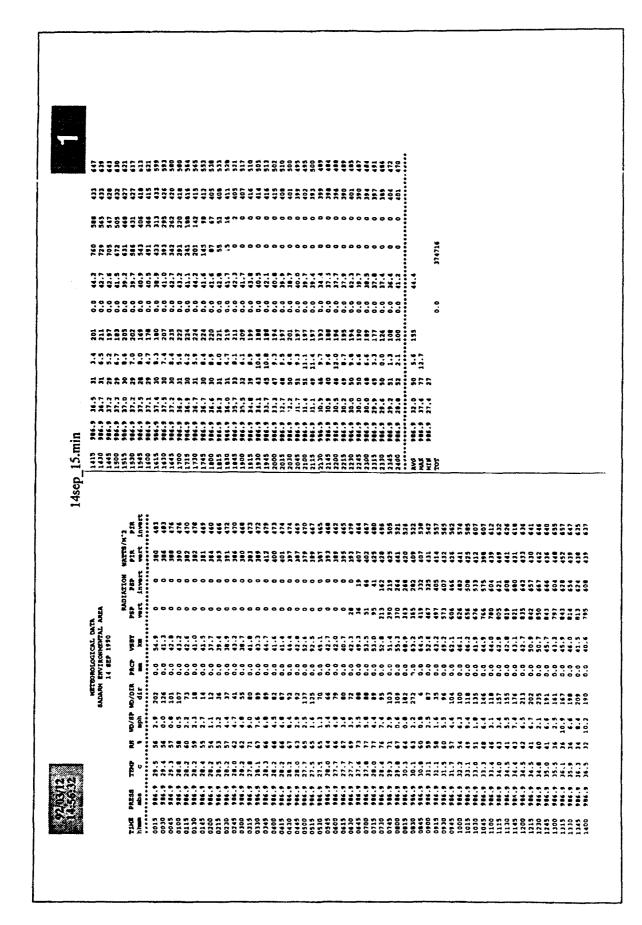
Parameter	instrument	Sensor Type	Range	Accuracy
Station Pressure Pressure	Sierra - Misco Model 1520	Aneroid Sensor Multi Cell	650 to 1,050 mbs	±0.2 mbs
Wind Speed and Wind Direction	R. M. Young	Speed - Tachometer Director - Potentiometer	0-50 m/sec 0-355	±2% ±2%
Temperature and Relative Humidity	Rotronic MP-100	PT 100 Ω RTD Capacitive Hygrometer	-50 to 150 °C 0 to 100%	±0.35 °C ±2%
Precipitation	Belfort Instruments Rain Gage	Tipping bucket	0" to 100"	±0.5%
Solar Radiometer	Eppley Precision Pyranometer	Thermopile	0.3 to 3 μm	±1%
Solar Radiometer	Eppley Precision Pyrgeometer	Thermopile	3 to 50 μm	±3%

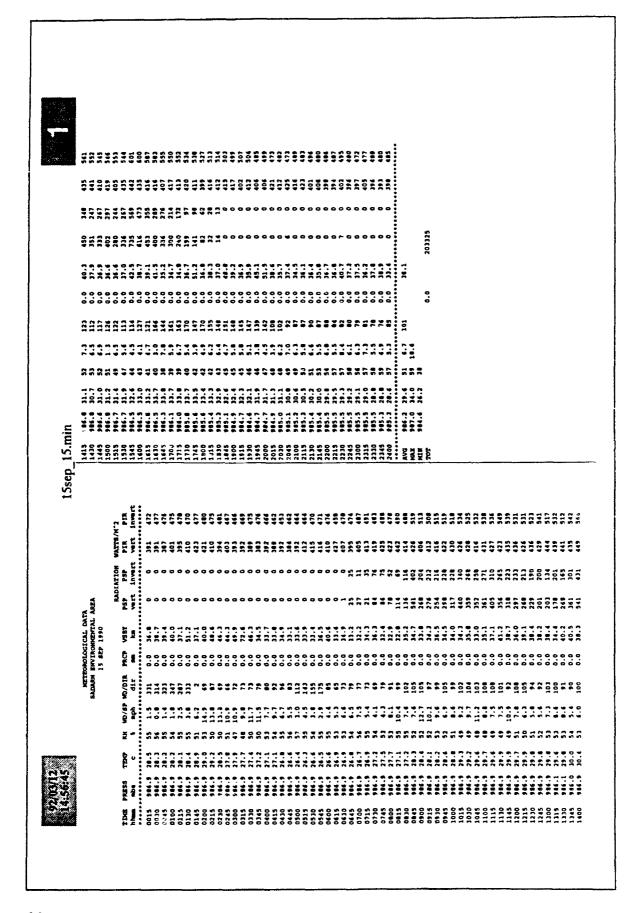


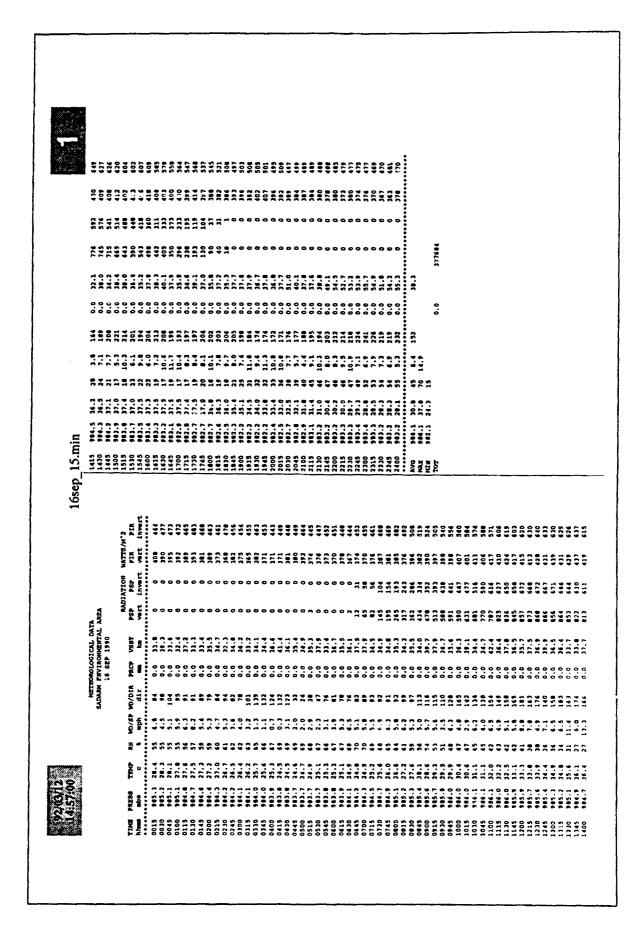


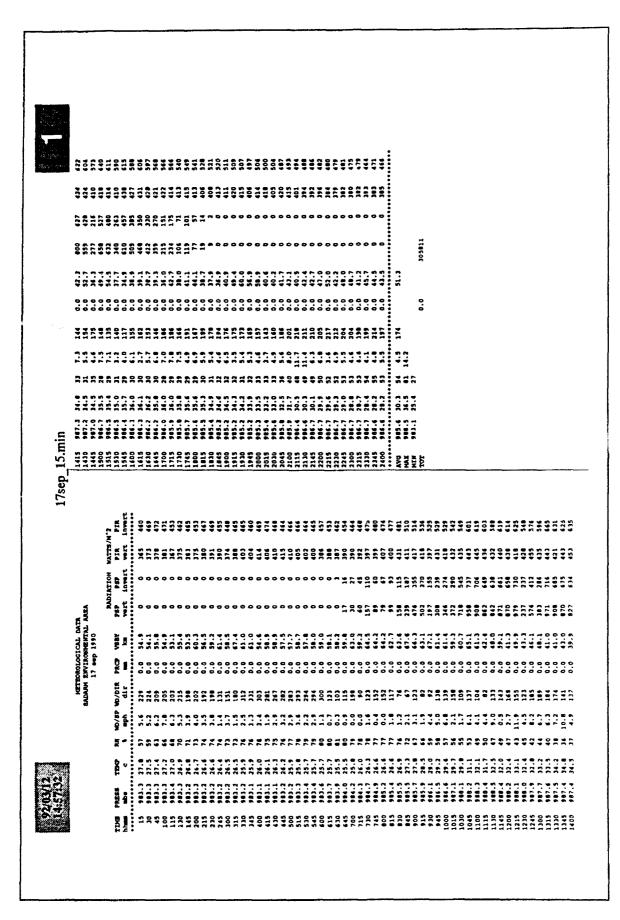


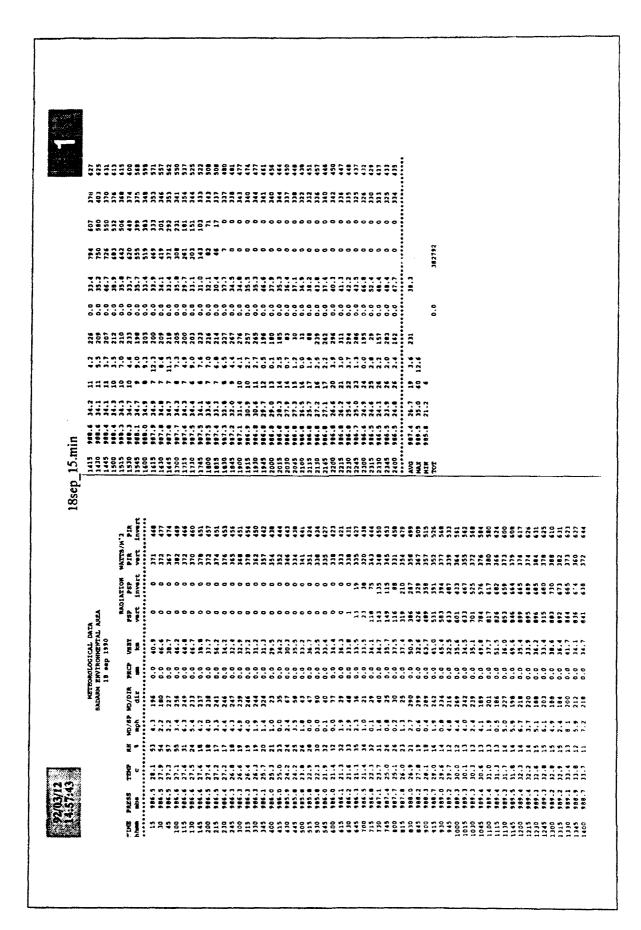


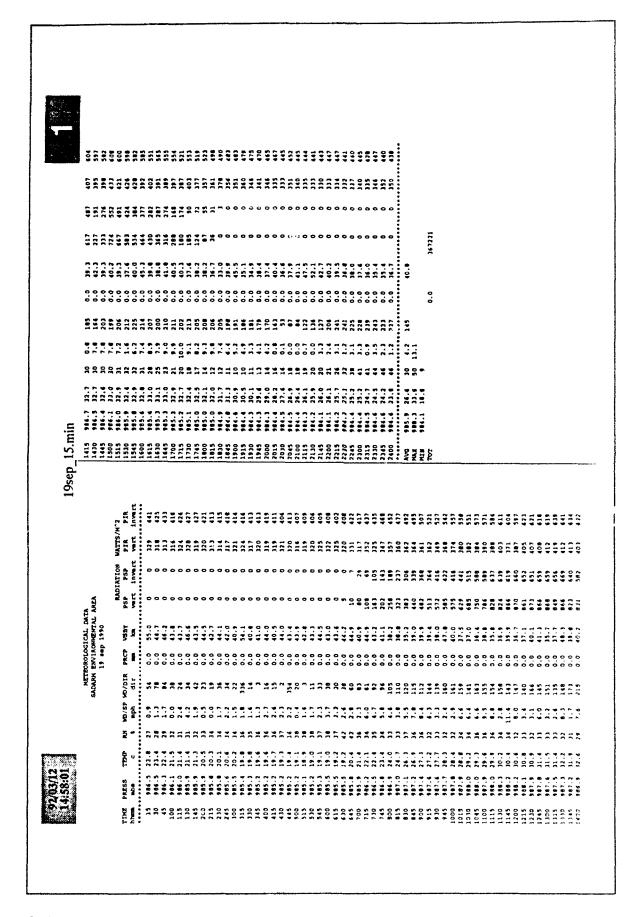


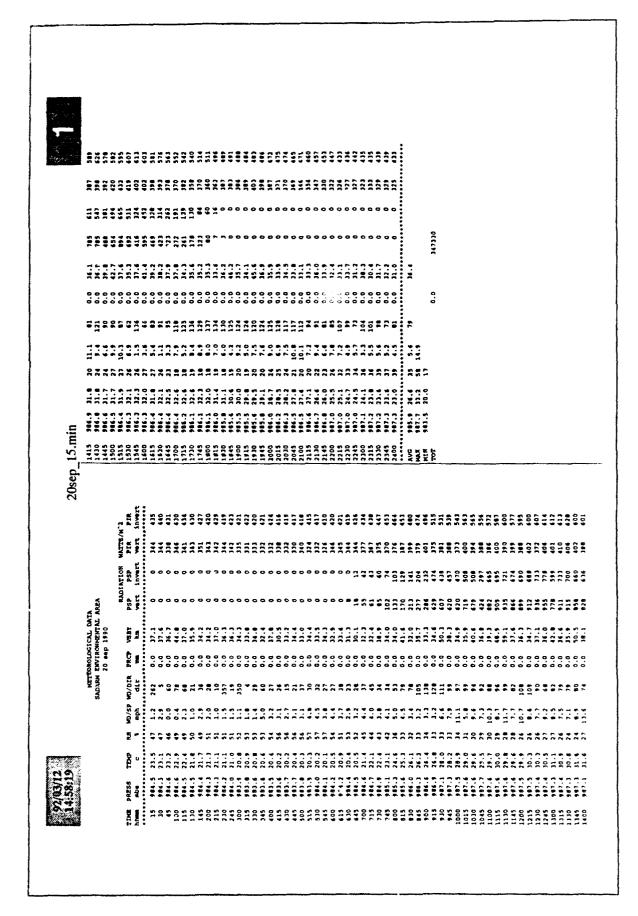


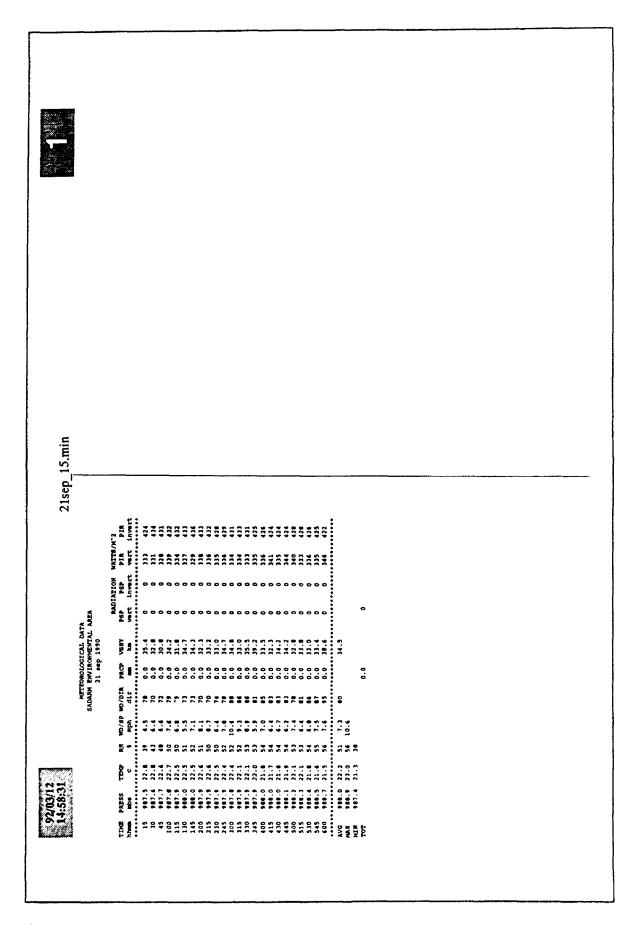


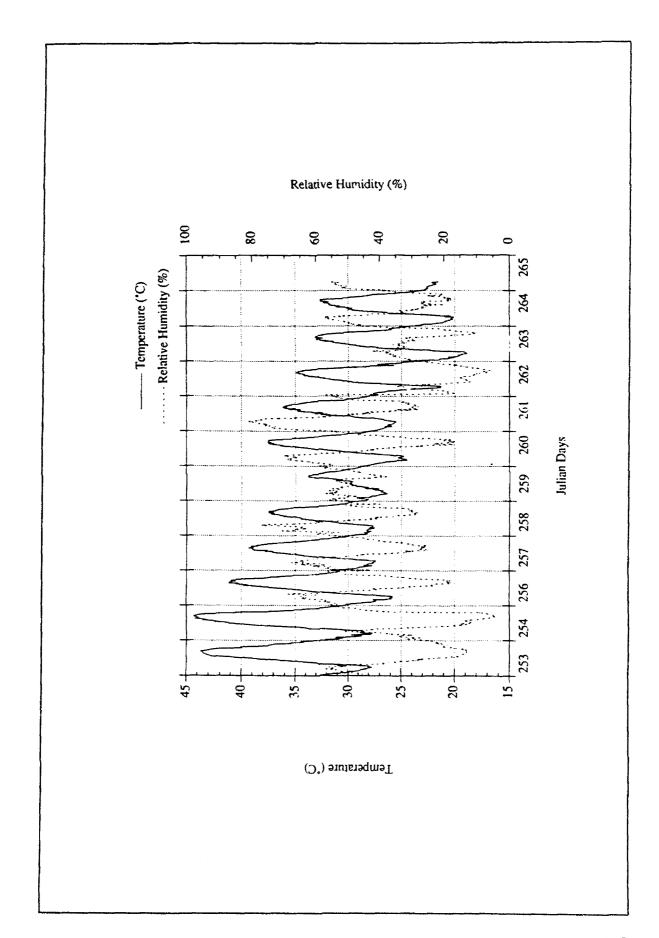


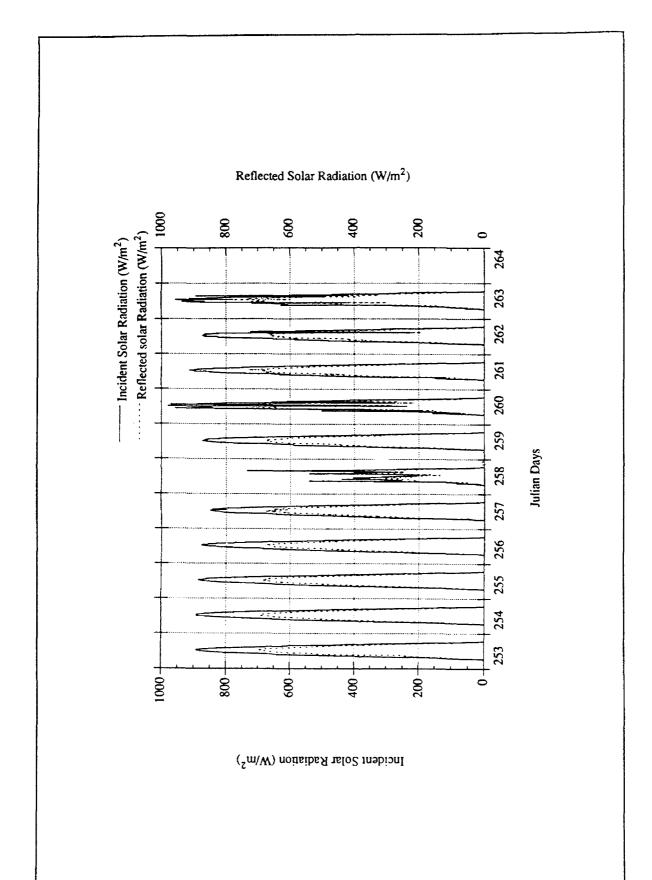


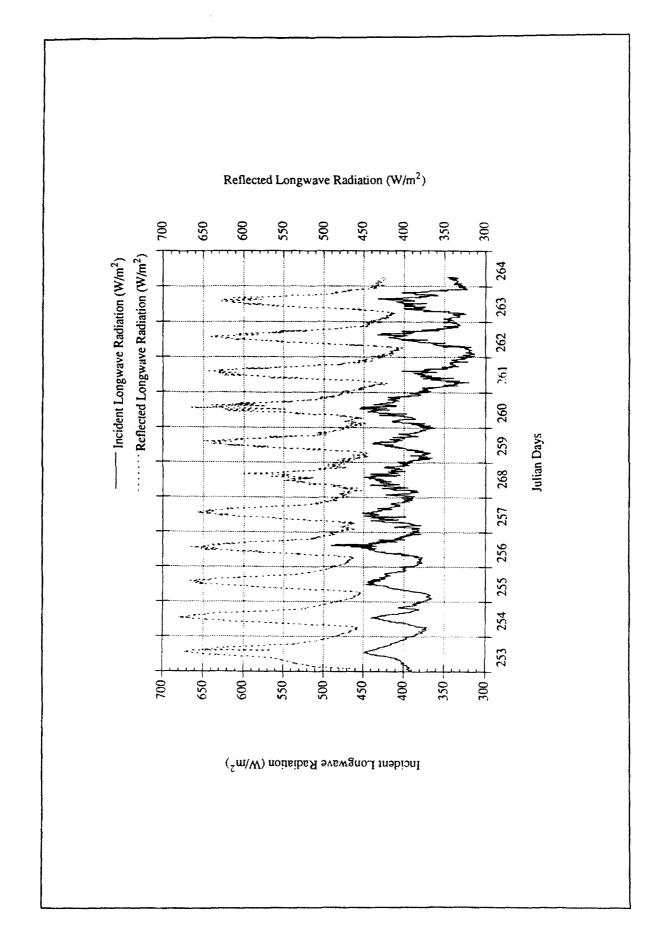










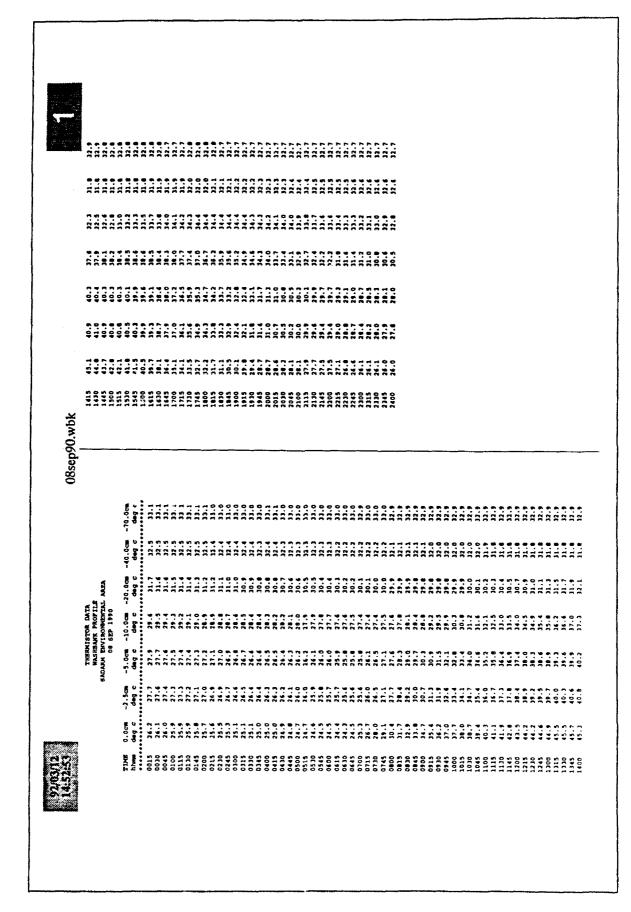


Appendix B Soil Temperature Profile Data

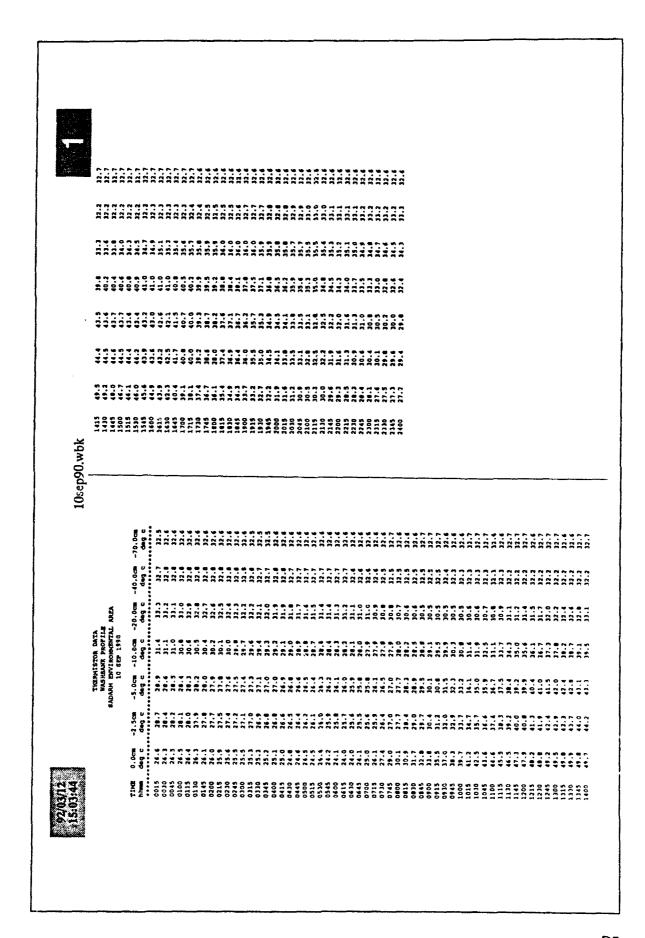
The following pages list soil temperatures (physical) recorded at several depths below the surface in two soil pits located within the Control Site near the Sense and Destroy Armor test area, Yuma Proving Ground, AZ. These data were collected during a 2-week period in September 1990. As with the data in Appendix A, these tabulations represent 15-min averages of 1-min data. Temperatures were measured with waterproof thermistors. The column headings indicate the approximate depth beneath the soil surface at which each thermistor bead was located.

There are two sets of tabulated data in this Appendix. One is identified by the ".wbk" notation and represents data collected in the wash bank pit. The other set is identified by the ".spf" notation and represents data collected in the pit located outside of the desert wash.

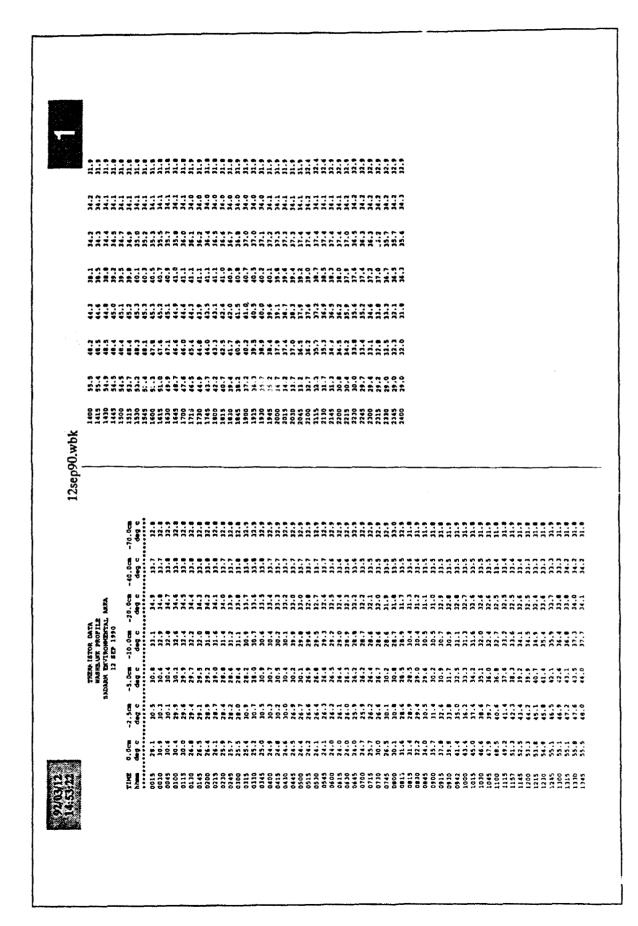
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07sep9												•													
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		-40.00m -70.00m deg c deg c	22.2	32.3	22.3	25.3	77	22	12.3	121	7 7 7	77.	7 7 7	. 5.	22	22.5	32.5	2.2	32.5		2.5	22.2			
	YAN TI	-20.0cm deg c	22.7	12.3	22.5	35.6	22.6	22.	22.5		111	9.00	35.6	22.5		35.5	22.5	7.7	32.		2				
	THERNISTOR DATA NASHBANK PROFILE SADAN ENVIRONMENTAL AREA 07 SEP 1990	-10.0cm deg c	22	34.7	22		7		77.	ä			77.7		7,	2	9.9.5	9.	20.5	200	29.9	2 2 2			
	THERM NASHBA SADANH ED	-5.0cm deg c	36.0	36.2	36.1	35.6	9.50	7		7.7.		10.0	200	2 % 3			20.5	28.7			79.7				
	-	-2.5cm dag c																				27.9			
		0.0cm deg c	;																						
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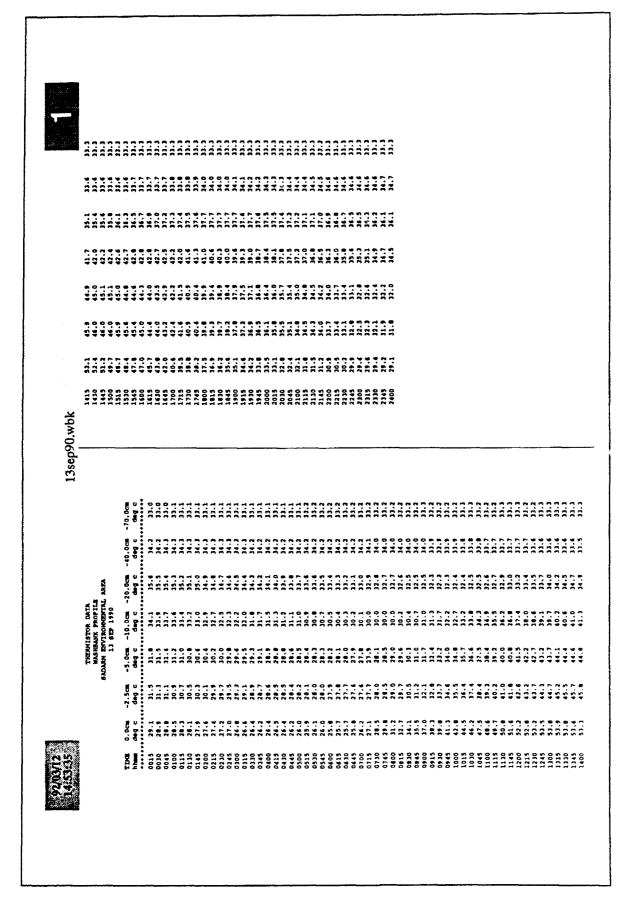


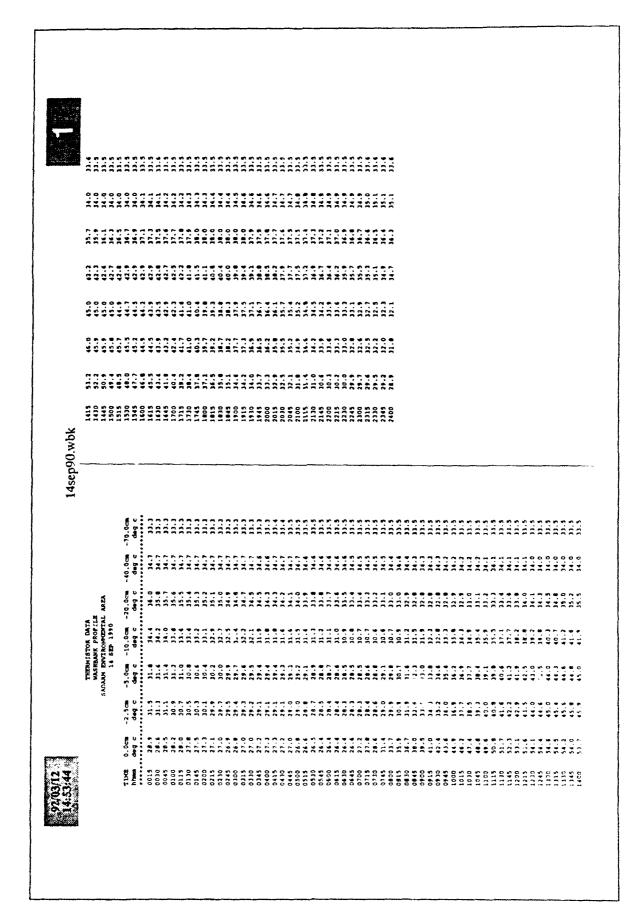
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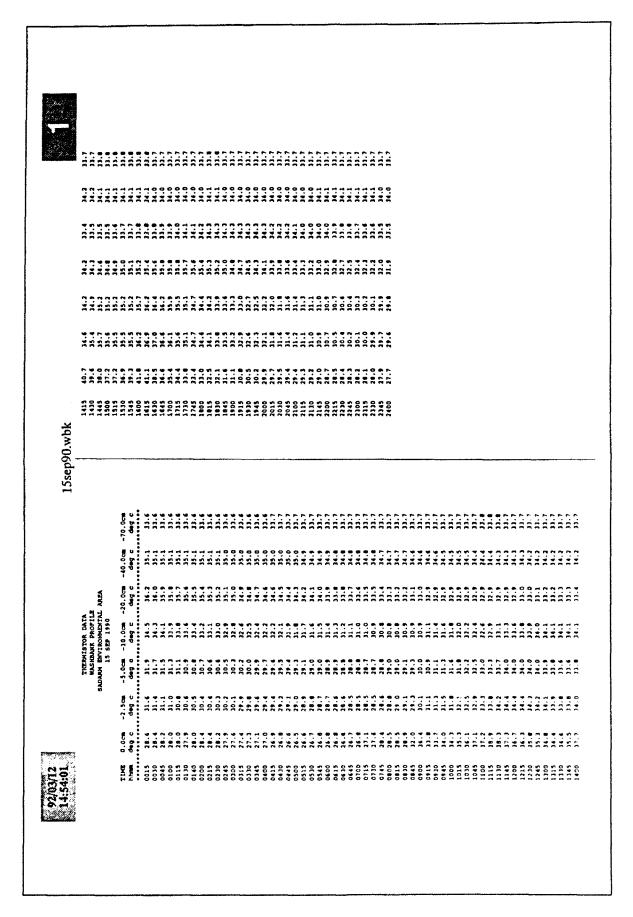


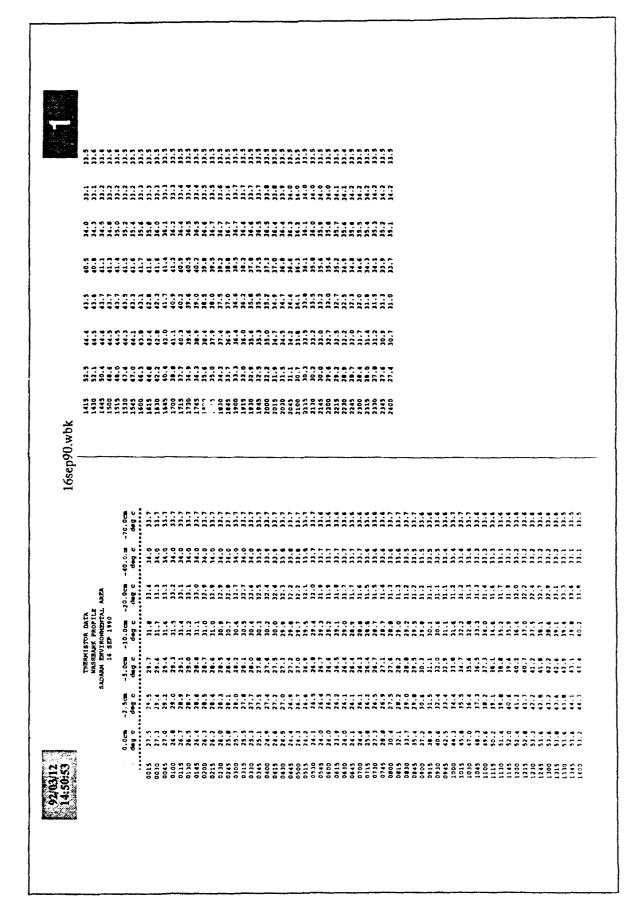
	32.0	22	32.8	32.6	22.0	12.7	32.0	12.6	32.6	72.0	12.1	22.7	27.5	32.0	12.1	12.7	32.0	32.4	22.0	32.0	77.7	12.0	12.6	12.E	33.6	32.0	22.4																		
	32.5	: : :	32.6	 	22.7	2.7	32.4	2.5	2.3	5.5	2.5	9.0	:::	27.5	?:		33.3		7	33.5	 		37.6	11.7	11.7	23.7	2.7																		
	32.3	9.7	13:1	15.1	23.7	36.0	36.2	7.7	3.5	¥.5		36.6	¥.4	36.5	5.5	, , ,	36.3	76.2	×.0	96.0		15.7	35.6	15.4 15.4	15.3	35.2	12.0																		
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	8.83 8.83 4.83			::	5.5	5 .3	7		39.7		3.3	6.7.	, o.	35.5	13.0	=	37.6	7.7	3.7	33.4	22.7	32.5	27.7	2.5	33.4	2.5	30.7																		
	51.4 50.4			: ::	:: ::	9	3.5	26.5	37.7	 	7.5	7.7	2.5	32.9	7.1	3.0	32.6	77.7	1	33.0	9 9	0.0		2 2	33.0		7.7																		
ьk	1415																																												
11sep90.wbk		·	*							•••				***																							• •=	_						_	
			-70.0cm		2.5	32.7	32.7	33.7	32.7		2.7	77.5	2	22.7	12.7	2.7	12.7	12.7	2	32.7	12.7	32.7	22.7	12.7	32.7	12.7	32.8	12.7	22.7	2.5	32.8	2 2	33.7	33.0			33.0	2.5	32.	2.5	32.6	2 2	2.0	32.0	32.6
			-40.00	1 000	2.5	2	13.3		13.3	::			: :	Α.		2	33.3		?	33.2	33.2	2.2	7 :	1.5	23.1	: :::	19.0	13.0	2.5	22.9	22.5	22.2	32.0	32.8	2 5		7.7	22.7	32.7	32.6	32.6	22.5	22.5	32.3	32.5
	3423				7.7	7.0	£ ;	7.7	33.6	: :	::	2.5	32.9	32.9	22.6	37.3	32.4	22.2	17.	33.0		1:3	===	7.1	11.4	: :	7	31.0	2.5	9	30.8	9 9	9.0	30.9	9 .	:::	31.3	Z :	• •	32.0	32.2	2	32.	33.1	7.50
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	THERMIN WASHEAU DARM ENVY	=	-5.0cm			23.5	23.0	28.5	38.3		23.7	27.5	2.2	27.3	26.0	7.	26.5	26.4	7.92	26.0	2 2	25.6	23.5	25.4	23.7	 %	27.7	27.8	• • • •	9.00	31.3	35.1	34.0	35.0		7.6	29.5	7.5		5.5	45.1	3 5	7	÷:	:
	6		-2.5cm		2.6.2	7	5. 5. 5. 5.	38.7	27.9	7.7	32.2	27.5	26.9	26.8	26.5	76.3	26.2	25.9	25.8	35.6	25.5	25.3	22.7	25.1	25.5	26.0	27.1	27.9	: :	30.	11.7	32.4	7	35.6	9.5	7	39.3	6 0.5		\$.5	7:		: :	ž :	
170.2000			0.00		27.0	26.5	 	23.6	25.5	5.7	25.1	23.0	24.7	2.		2.5	24.3	23.8	23.7	23.6	22.5	23.3	22.	7.7	32.6	. ; ;	39.0	30.	7.5	3.6	17.1	. C	9.	42.9	? ;		47.5	5 5	4.0.0	50.7	51.2	7 5	5.5	52.2	52.2
3:13			#14E		2100	0043	0100	0110	0145	0200	0530	0245	9315	0330	0070	6190	00.30	0500	0513	0530	0500	0615	06.30	0100	0715	0730	0000	0815	0.00	0060	0915	6 5	1000	1015	1030	1100	1115	1130	1200	1215	1230	1245	1315	1330	1345



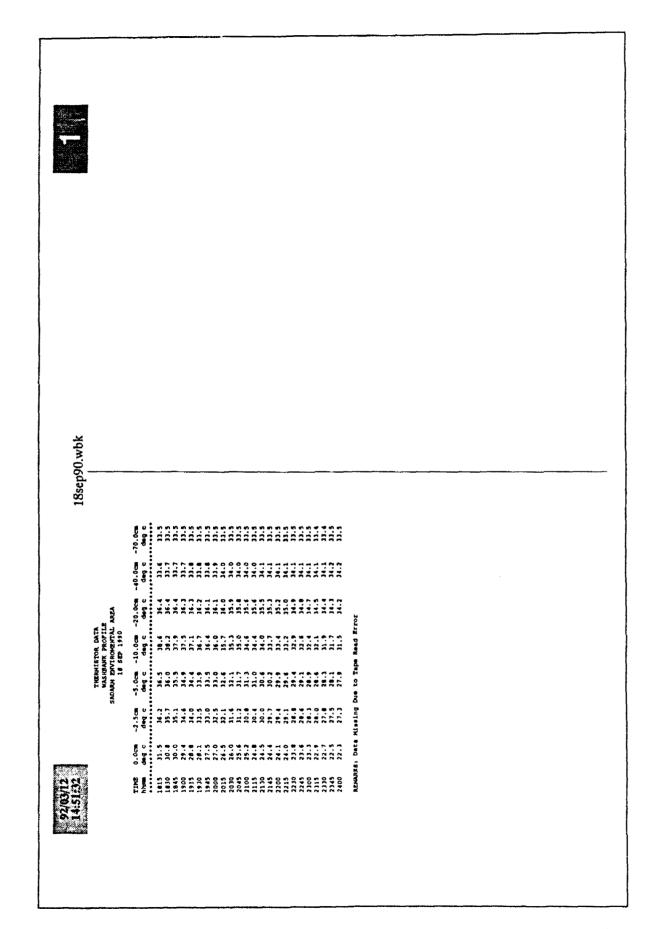




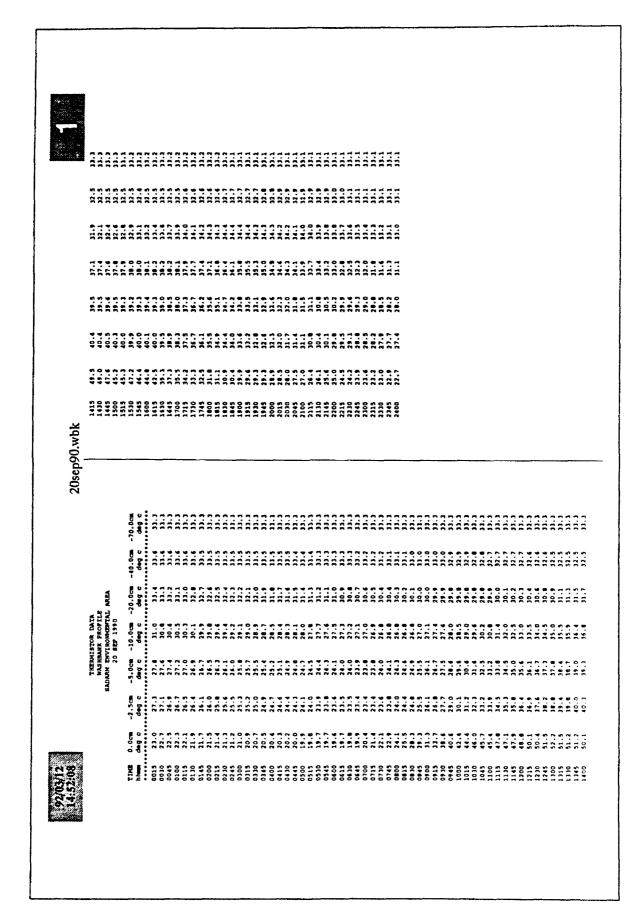


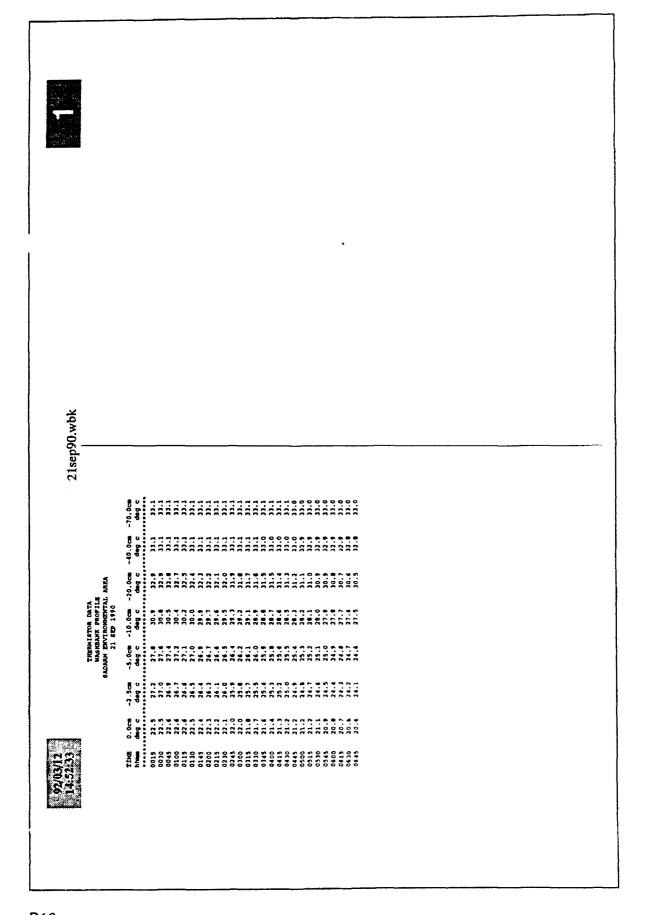


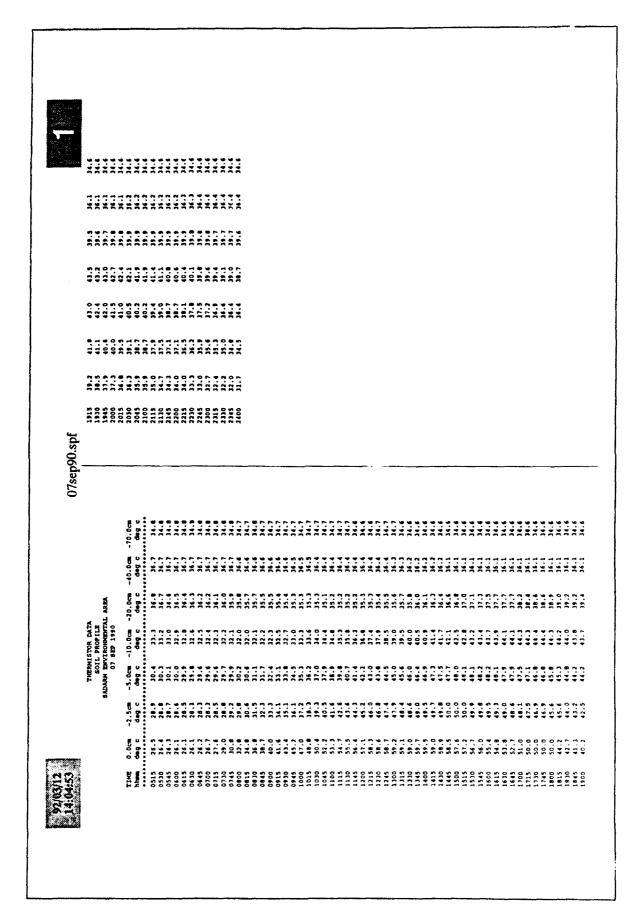
	222	2 2	32.6	32.	2.2.	32.7	32.7		32.0	33.	2 2	7.7	2.5	77.7	32.0	2 :	72.	22.7	2:	77.	32.8	2	32.6	32.6		32.8	32.	72.7																		
	200	2 2	2 2	12.9	2.5	22.9	32.0			12.4		12.5		77	32.9	5.5		33.6	6.5		32.9	5.5	33.0	33.0	9 5	9.6	0.0	37.0	•																	
	12.1	77.7	12.9	33.0	2.7	3.4	33.5		=	7.7	? :	=	::		34.8		15.0	3.0	13.1	2.5	13.1		15.1	33.7		13.0																				
	35.4	7 7	7.7	2.5	37.6	17.5	9.0			 	:	7	÷;	7.7	37.5	?;	7.5	¥.	ž.		35.0	9.7		33.0				2.0																		
	33	5.5		42.6	5.5	5.2	5.0	: :	=	60.0	÷	3	 		37.3	7.7		2.5	33.1		7.	2.5		3.0	2.7	2.0			:																	
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	1430	1500	1515	1545	0091	97	1645	1700	1730	1745	000	000	1045	200	1930	1945	2000	200	2045	2116	23.30	2145	2215	22.20	2245	2315	2330	2345																		
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			-2.50	deg c		10.0	10.1	29.9		29.6	2.5	7	29.0	 	7.7	38.8	÷.		2.	, ,	2.3	78.3	?	28.0	27.9	27.5	26.0	78.5	20.6	78.6	29.0	30.0		32.0	32.3	32.6		, e	3.6	• • • • • • • • • • • • • • • • • • •	42.1	4.5			÷.	;
<i>0000</i>			0.00	0 500		22.0	26.9	56.9	7. 7.	7.	26.6		26.5	7.7	7 7	26.3	26.3		36.6	\$ 7		26.3	7. 5	2 2	25.6	7 %	27.7	7.5	79.7	29.1	2 2	35.7	76.7	2 2	16.7	* :		=	•	•	50.7	20.3		50.6	52.3	S :
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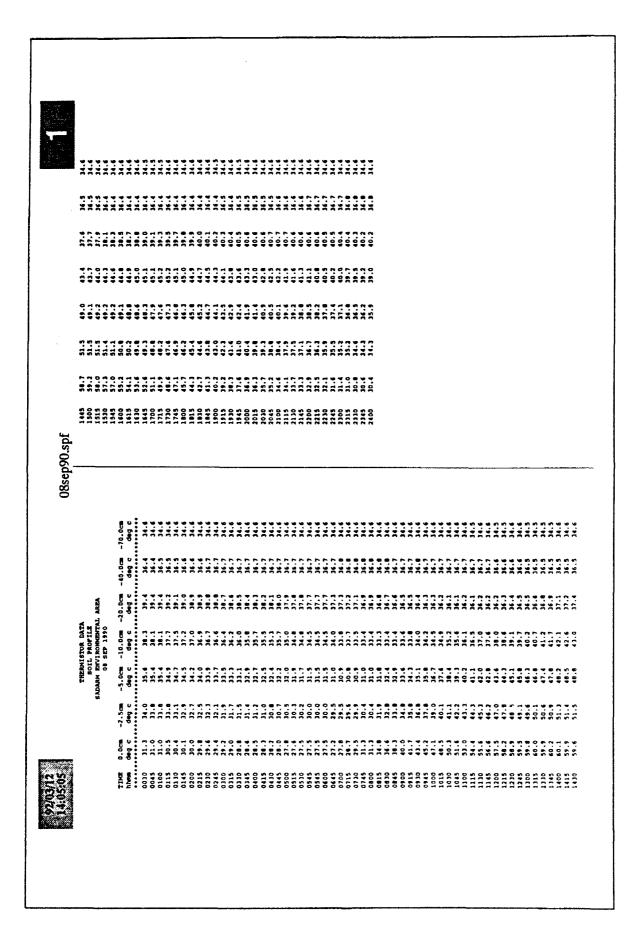


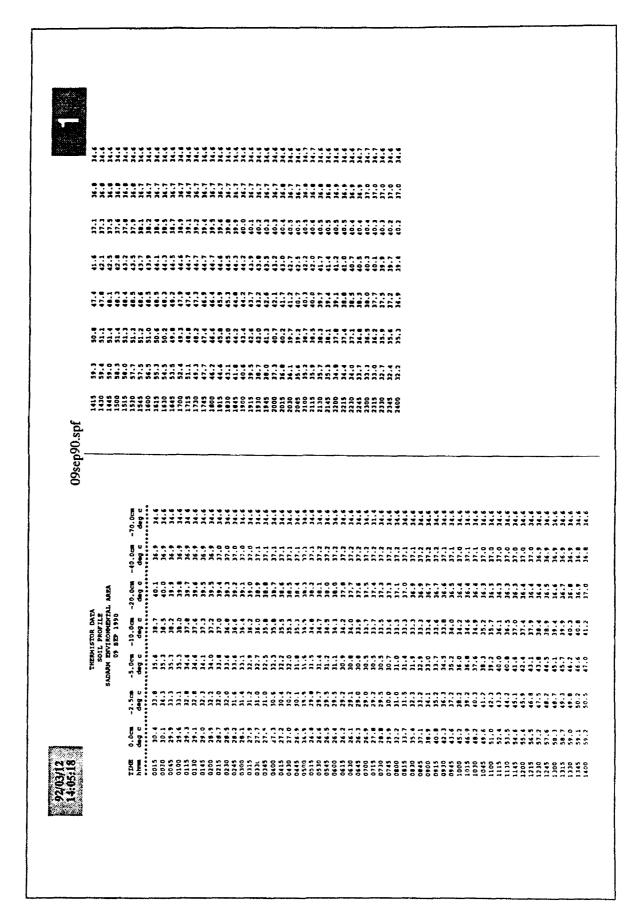
() V																																						
	55555	22.		7.5	1.1	33.4	2	7.7	7.7	2.5		i.	33	22.7	2	22.7	2.5		22.7	2:		33.3																
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	7.5.2.7.2				33.0	35.1	15.3	13.1	35.4	2.5	15.2	33.2	35.2	35.0		74.7	5.5	7.7	7.5	2	7.7	33.6																
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	STOR DATA HE PROFIL TRONGENTA SEP 1990	-10.0cm	. ~ .		30.5	2.5	3 2	29.5	2	28.8	20.6	7 9 .7	28.1	27.	27.5	27.3	27.0	26.9	2.	7. 7. 7. 7.	2	7 7	26.5	27.0		1.3		23.3	5.02	31.0	32.5	17.7	34.3	35.5	0. Y	3,70	7.	39.2
	THENISTON DATA MASHBANK PROFILE SADARA ENVIRONMENTAL ANEA 19 SEP 1990	-5.0cm		27.7	26.9	7.	7 0.	25.6	2	23.1	27.3	5.5	7.7	7.0	 	23.6	23.4	23.2	23.0	23.0	2.5	7	28.0	36.7	9.6	33.3	20.5	17.7		¥.	35.6	17.0	17.7	2 5	£ ;		9.0	- 7 - 1 - 1
	જ	-2.5cm deg c	•	26.6	26.1	23.3	25.4	25.2	2	24.5	24.3	. 0.	23.6	23.5	23.5	2	22.9	22.7	22.5	22.5	22.9	24.2	 	36.1		29.1	30.	12.7	7.7	35.6	36.4	17.	£ .		40.4	£0.	: n	7.7
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net com		TOG	\$100	0043	0100	01.10	0200	0215	0245	0318	0130	0400	0415	0.0	0200	0830	0000	0615	06 65	0700	0730	0080	0818	00 45	0060	06 90	0000	1015	1010	1100	2111	1145	1200	1230	1245	1300	1330	1345
77/00/17 14:51:49																																						

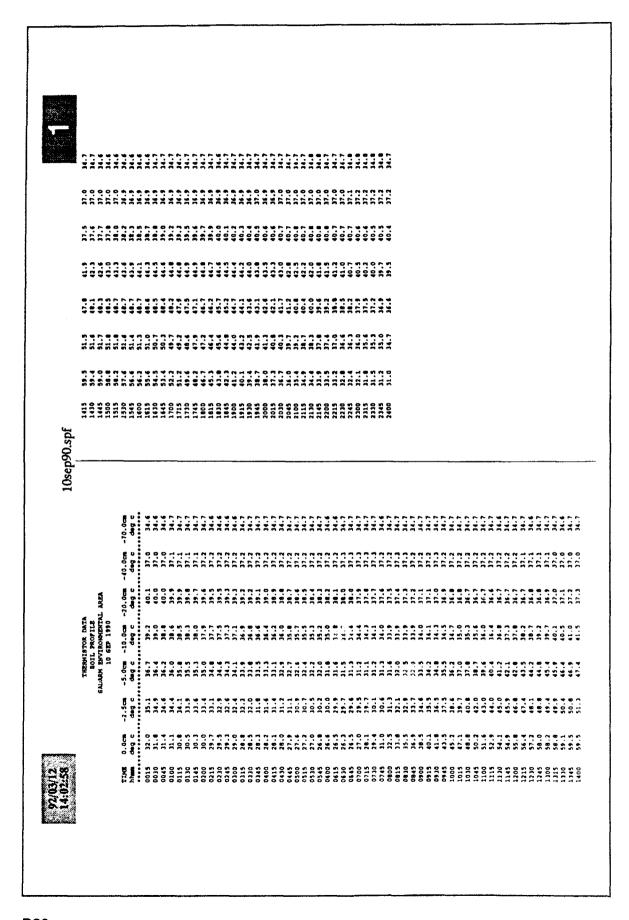


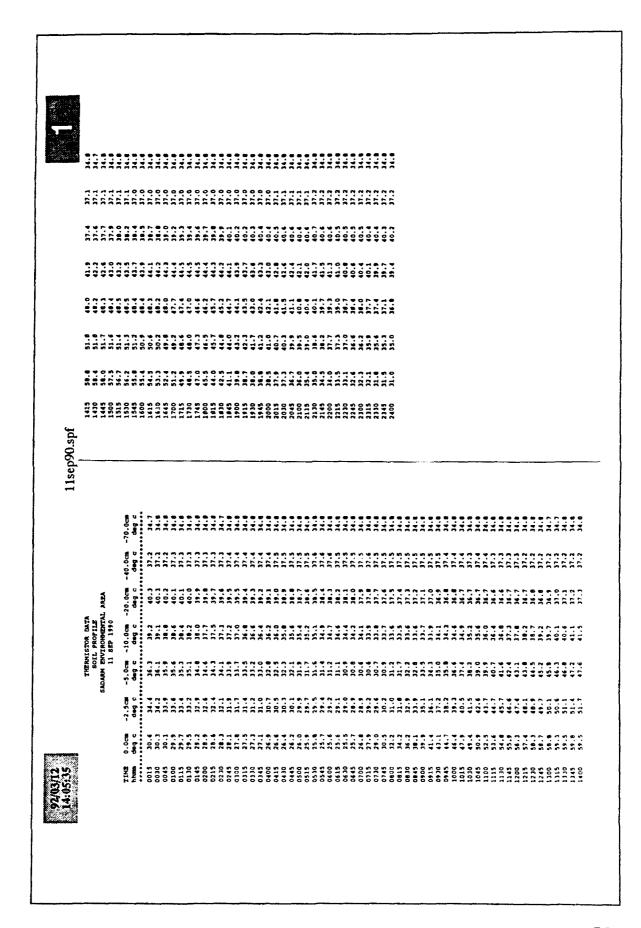


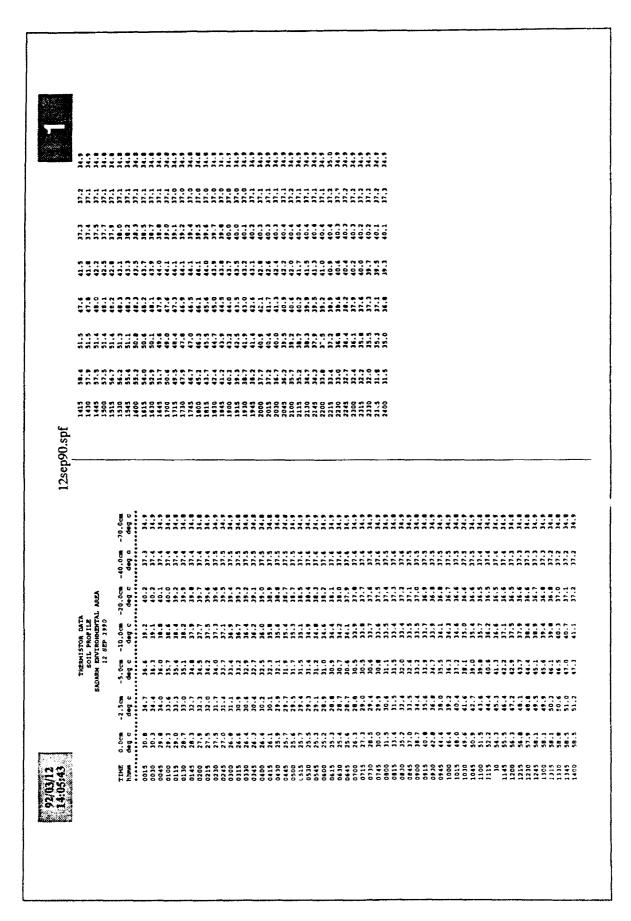


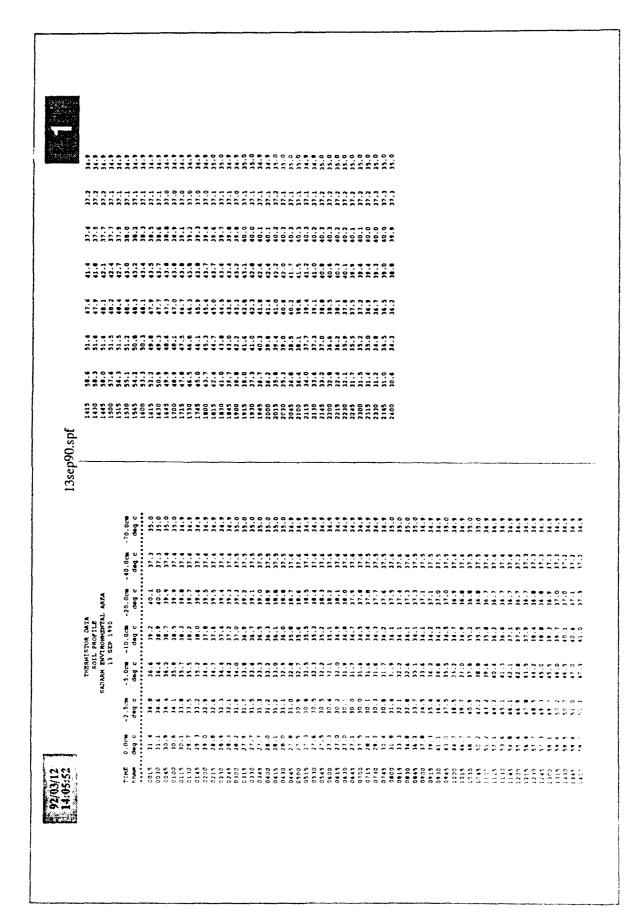


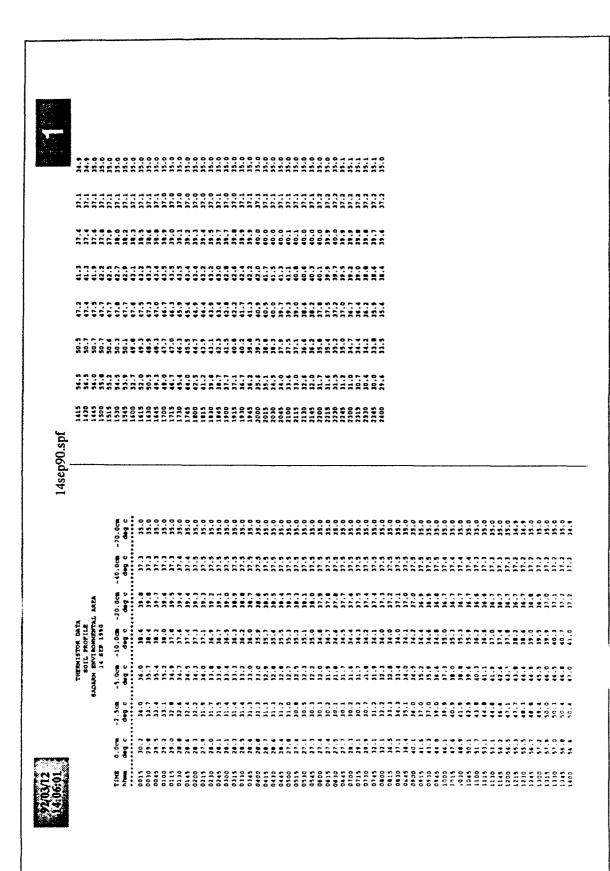


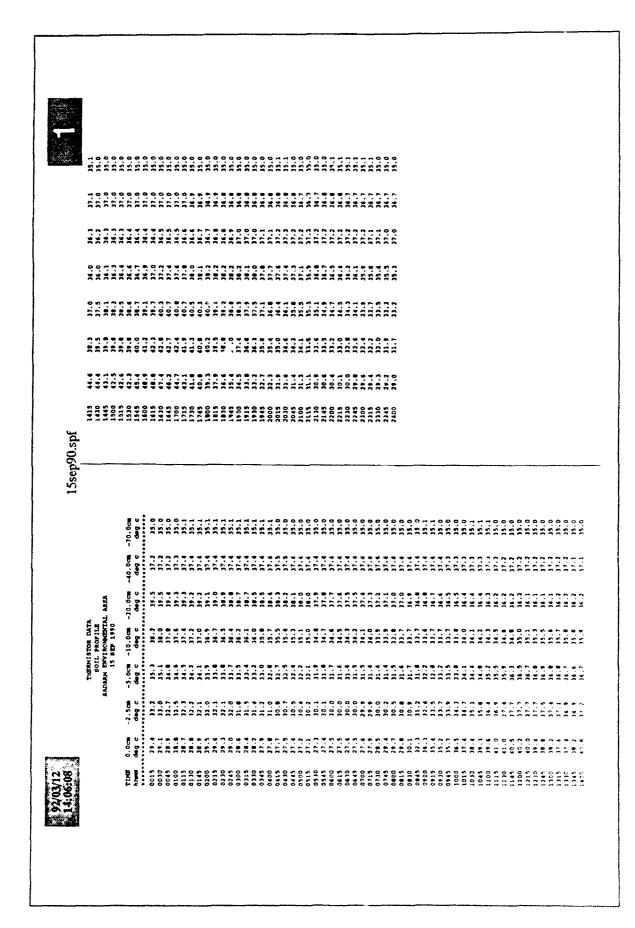




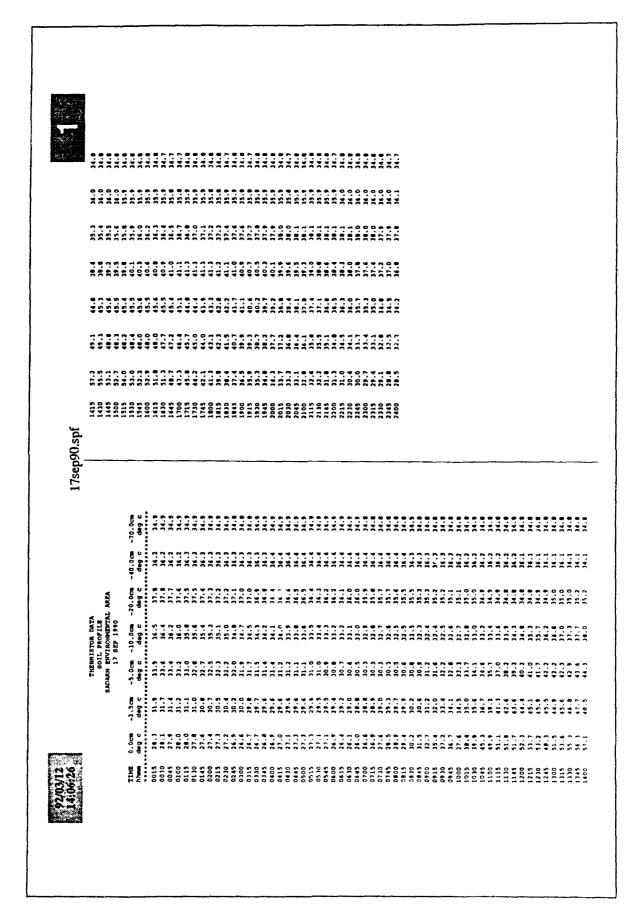


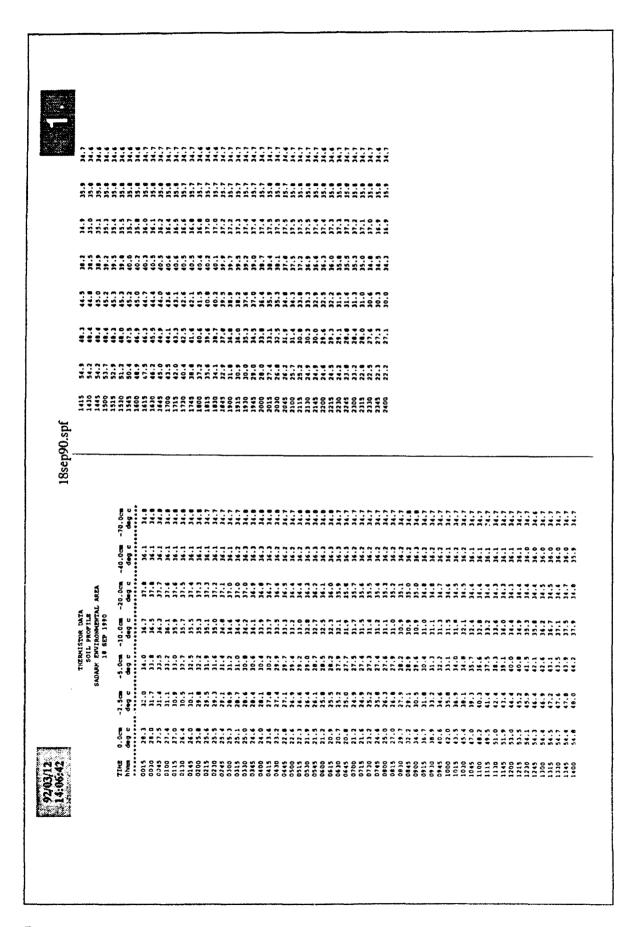


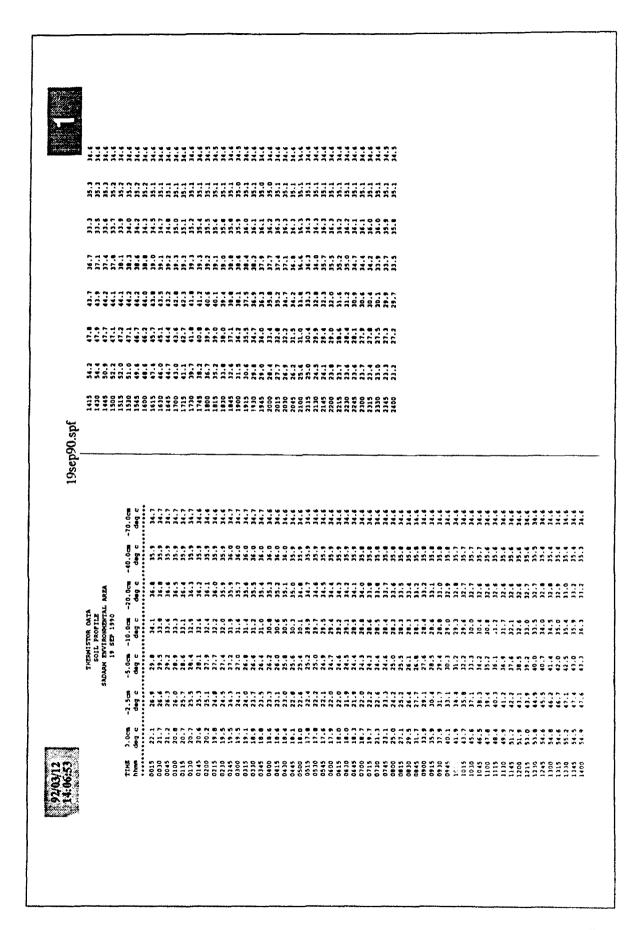




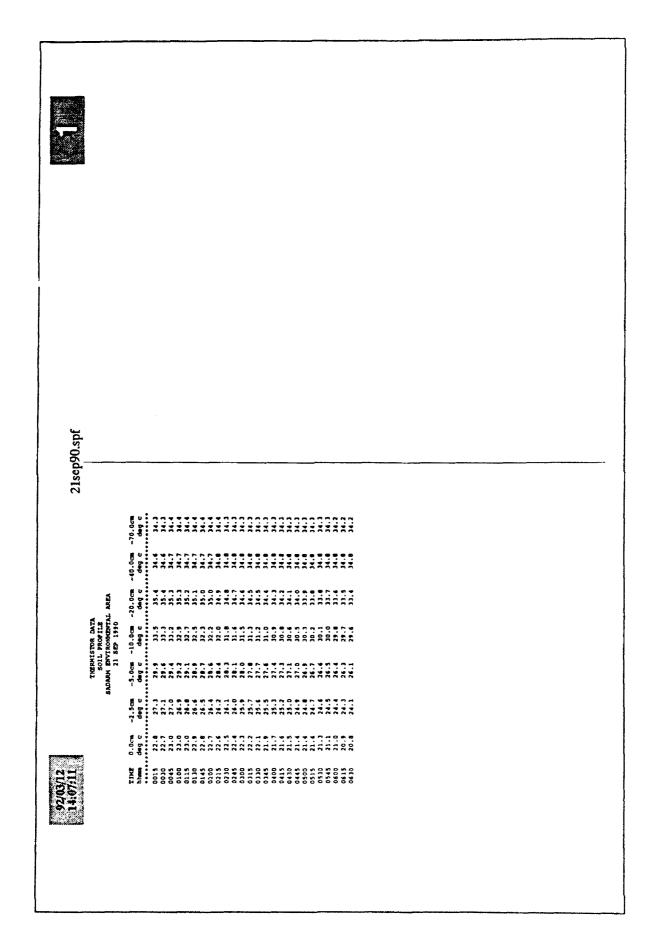
	15.0	36.9	36.9	36.9	34.5	34.9	24.9		7.0	34.9	9.70	7.5	34.9	34.9	, X	7.0	36.9	35.0	33.0		34.9	÷.	25.0	9.9	96.9			34.9	16.9																			
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1414	123	1515	1945	1600	1630	1649	1700	17.19	1745	1800	519	1163	1900	200	2	2000	2013	2030	5043	2115	2130	2165	2215	2230	2245	2300	2330	2345	200																			
<u></u> -		,	o Beg		35.0	19.1	35.1	15.1	35.1	35.1	35.1	35.0	35.0	35.0	35.0	35.0	33.1	35.1	35.1	35.1	38.1	35.1	9.00	15.0	15.0	0.50	13.0	15.0	35.0	13.1	35.0	35.0	35.0	35.0	0.00	35.0	33.0	0.5.0	35.0	35.0	94.9	35.0	35.0	35.0	34.9	36.9	3.0	33.0
			deg c		7 %	76.7	76.7	· ·		36.7	7.7	36.7	36.7	36.7	· ·	76.7	7. 9.	36.7			36.7			7.	36.6	* *		9.90	9. 9.	9.9	9.	? *	3.	 	7. 7.	36.4	16.4	· ·	, <u>, ,</u>	×.				36.2	~ ;	7 . 7	7 9 7	7.00
	L AREA	ļ			7	ž.	96.9		16.7	36.6	9, 9	36,5	36.4	36.3	: :		7.90	16.1	e :		15.0	2.5		35.5	13.4	2 2	2.5	23.7	13.0	35.0	6.5	 	7.	¥ :		2.5	£.5	: :		34.5	 		7.	34.1	- :		25.0	1.00
arton para	SADARH ENVINONGENTAL A	0661 429	0 000	٠,	35.1	35.0	7.	 	: :	34.3	7.7	7 0	33.6	33.7	÷ :	7.5	13.7	11.1	2.5	2.7	32.5	32.5	3.5	92.0	1.1	= -		3.5	9 5	31.3	: :	2.5	=	22.0	12.5	2	2.2	2 :	7	7.7	73.5	2 2		37.0	7.5		7 97	P 7
10000	601 BADARM EN		, i		22.5	32.0	3.5	2 :	32.0	1.1	1.7	7.1	31.2	31.1	9.5	30.0	30.4	30.2	9 5	2.5	29.8	2.5		2	29.0		. 6	39.1	23.7	3.2	•		37.7	2	: :	36.0	5.3	7.7	5.5	40.7	\$ 0,			÷:	÷ :			2.0
		•	deg e	;	7:7	1:1	9,0	2 9	30.4	30.2	 2	29.7	29.5	29.1	? ;	28.7	7.02	20.2	9 .	27.6	27.6	27.5	27.5	27.7	27.3	27.2	27.7	28.2	28.8	30.3	7.	7 7	¥	Z :	3.0	2	40.5	÷ ;		¥.5	9.0	•		47.5	0.			2.
			0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	•			27.5		27.5		7.7		7.4.4	26.3	2 2	· ·	24.9	74.7	# X	2.5	24.5	7.7	2 2						10.9																			
						-	0	•	•	0	•		o		9 4	2 2	2	2	2 9	2 20	2	2 9	<u>.</u>	2	•	0000	2 2	2	2 2	2	2	2 5	2	2	<u>.</u>	9	•	g v	. 0	*	o	•	, ,	0	•		n (0





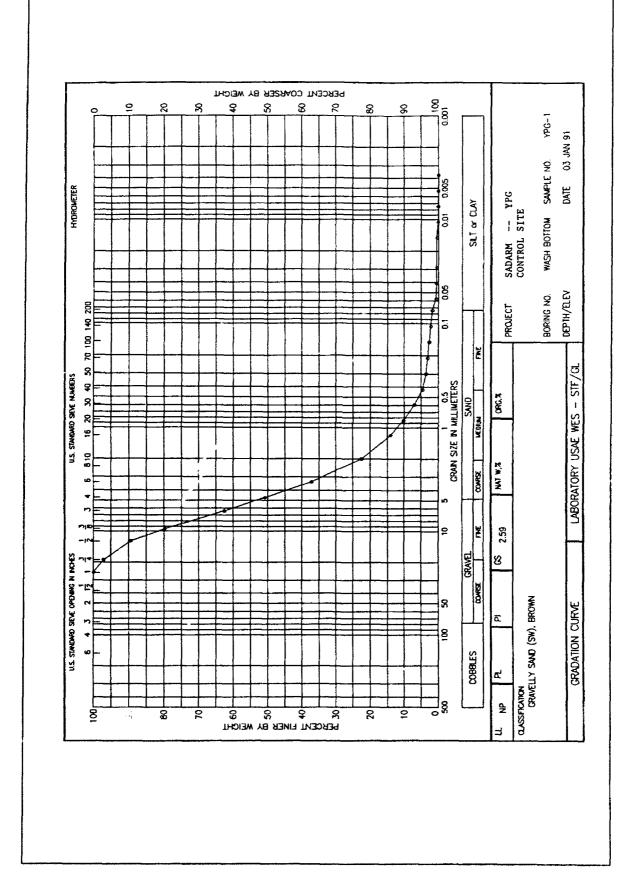


		, , , , , , , , , , , , , , , , , , ,		77.	7.7	34.3	7	7		:::	7.7	7.7		7.7	7.7	36.4	7.7	7	7.7	7.7																
;	7777	. 4. 4.		7.7. 7.7.	24.5 24.5	34.5	3.5			, 4 , 5 , 6	24.5	7.7	: :: : : :	. s.	 	3. 5. 3. 6. 6.	7. X		9.5	7.																
;	22.5			34.1	7.3 7.3	34.6	34.9	35.2	35.4	35.5		7.57		35.0	9.50	35.8 35.7	72.7	2.7	33.6	15.5																
;	96.2 86.2 86.2 86.2 86.2 86.2 86.2 86.2 8	######################################		5. F.	2.7	7.8			7.7.	37.7	2, t.	97.0		 	2 S. S.	35.5	35.0		7.0	3.5																
:	25.5	25.0		5.5	45.2 42.1	5.5	7.0	39.1		35.1	35.5	13.4	7.	7.5	11.	32.7		11.2	30.8	30.2																
;		8 8 8 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4		T 7.	2.5 2.6	42.6	3.6		36.4	36.4	2.50	13.5	5.2	32.0	10.7	29.7	29.3	2	20.7	27.6																
	\$2.7 \$0.0 \$0.0	22.5	# # # # # # # # # # # # # # # # # # #	5.1.5	2.5	39.7	35.9		12.5	11.1	30.6	39.4	7	27.5	% % % %	25.2	22.5	::	23.7	23.0																
;	1415 1415 1465 1500	1510		1445	1715	1745	5	1865	1915	2 2 3	2000	2030	2100	2132	21 45 2200	2218	2245	2315	2 2	7400																
20sep90.spf																																				
		100 B		7. t. t	4.6	9.5			 	2.5 2.5	9.9			. s.	? ? ?	5.2 5.3	5.	. s.	 	:			? :	-		**	: :			:	• ·	::	*			
		.0cm -70.0cm	35.2 34.6 35.2 34.6		35.3 34.6 35.3 34.6	35.3 34.5	35.3 34.5	15.1 34.5	35.3 34.5 35.3 34.5	35.3 34.5 35.3 34.5	35.3 34.6	35.3	35.3 34.5	35.3 34.5 35.3 34.5	35.3 24.5	35.3 34.5 35.3 34.5	35.3 34.5	15.2 14.5					• • •				, .,	, -,	.,	•		_		34.8	34.4	
	ร ม	-40.0cm deg c	35.2	13.5 13.5					34.6 35.3 34.5 34.7 35.3 34.5	34.6 35.3 34.5 34.5 35.3 34.5	34.5 35.3 34.6	34.3 35.3 34.6	34.1 35.3 34.5	34.0 35.3 34.8 33.9 35.3 34.8	33.0 35.3 34.5 33.7 35.3 34.5	33.6 35.3 34.5 33.6 35.5 34.5	. .		15.2		35.2	15.2	32.5	2.5	13.1	17.51	0.51	38.0	35.0	34.9		_	37.8		32.4 34.0 34.4	
	ONE DATA HOPTLE POWEDIAL ANEA P 1990	-20.0cm -40.0cm deg c deg c	35.0 35.2 35.7 35.2	35.6 35.3 35.5 35.3	35.5	35.3	33.	34.9	7.7	30.9 24.6 35.3 34.5 30.7 24.5 35.3 34.5	34.5		7.7.	33.0	33.4	33.6	31.5		15.2	33.0	35.2	32.8 35.2	32.5	32.5 33.1	0 32.3 25.1	32.3 35.1	32.2 35.0	38.0	12.2 35.0	32.2 34.9	32.2 34.9	32.2 34.8	32.2 34.8	32.3	3,4	12.7
	THERMISTOR DATA 401L PROFILE DARW ENVINORHERTAL AREA 20 SEP 1990	Ост -10.0cm -20.0cm -40.0cm 19 с deg c deg c deg c	35.0 35.2 35.7 35.2	1 32.9 35.6 35.3 9 32.7 35.5 35.3	35.5	.3 32.1 35.3	33.0 35.5	34.9	7.7		30.6 34.5	30.3	30.0	29.7 33.9	33.4	29.3 33.6	29.0 33.5	28.0 33.3	26.7 33.2 35.2	1.00 O.00 O.00	26.6 32.8 35.2	20.4 32.0 35.2	20.9 32.6 35.1	20.6 32.5 35.1	29.0 32.3 35.1	29.2 32.3 35.1	29.9 32.2 35.0	30.3 32.2 35.0	11.0 12.2 35.0	31.5 32.2 34.9	31.9 32.2 34.9	32.7 32.2 34.6	33.1 32.2 34.8	32.3	2 34.5 32.4 34.8	15 1 12.7 14.8
	TREMISTOR DATA SOLL PROFILE SADAM ENTROMEDITAL AREA 20 SEP 1990	m -10.0cm -20.0cm -40.0cm c deg c deg c deg c	29.5 33.3 35.8 35.2 29.3 33.1 35.7 35.2	29.1 32.9 35.6 35.3 26.9 32.7 39.5 35.3	20,7 32,5 95,5 20,8 32,3 55.4	28.0 31.9 35.3	2.75 B11 B11 B11 B11 B11 B11 B11 B11 B11 B1	27.7 31.4 35.0	27.3 31.2 34.6	26.9	26.6 30.6 34.5	26.3 30.3 34.3	26.0 30.0 34.1	25.8 29.8 34.0 25.7 29.7 33.9	25.6 29.5 33.0 25.5 29.6 33.7	25.00 250.00 23.60 255.00 250.00	25.2 29.0 33.5	25.1 28.0 33.3	25.2 26.7 33.2 35.2 26.1 26.6 19.1 16.2	25.4 24.5 May 0 May 1	26.0 20.4 32.9 35.2	26.5 20.4 32.0 35.2	27.6 20.5 32.6 35.1	28.3 28.6 32.5 35.1	30.2 29.0 32.3 35.1	31.3 29.2 32.3 35.1	33.3 29.9 32.2 35.0	34.2 30.3 32.2 35.0	34.9 30.7 32.2 35.0	36.4 33.5 32.2 34.9	37.0 33.9 32.2 34.9	38.5 32.7 32.2 34.6	39.3 33.1 32.2 34.8	40.0 33.6 32.3 34.8	41.2 34.5 32.4 34.0	42.0 15.3 12.7 14.8
	TREMASTOR DATA SADAM ENTROPEDITE, AREA SADAM ENTROPEDITE, AREA SADAM ENTROPEDITE, AREA	-5.0cm -10.0cm -20.0cm -40.0cm deg c deg c deg c deg c	27.1 29.5 33.2 35.6 35.2 26.9 29.3 33.1 35.7 35.2	26.7 29.1 32.9 35.6 35.3 26.5 28.9 32.7 35.5 35.3	26.2 20.7 32.5 35.5 26.0 28.5 32.3 35.4	25.7 28.3 32.1 35.3 25.5 28.0 31.9 35.2	25.4 27.9 35.6 35.5	25.0 27.5 31.4 34.9	24.8 27.3 33.2 34.8 24.6 27.3 33.0 36.7	24.4 26.9 24.2 26.7	24.2 26.6 30.6 34.5 24.1 26.4 30.4 34.4	23.5 26.3 30.3 36.3 30.5 4 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5 5.5	23.6 26.0 30.0 34.1	23.5 25.8 29.8 34.0 23.4 25.7 29.7 33.9	23,3 25,6 29,5 33,8 23,2 25,5 29,6 33,7	23.1 25.4 29.3 33.6 23.1 25.3 29.1 33.6	23.0 25.2 29.0 33.5	23.2 25.1 28.0 33.3	23.6 25.2 26.7 33.2 35.2	26.3 25.4 20.5 33.0	25.6 26.0 20.4 32.8 35.2	26.7 26.5 20.4 32.0 35.2	20.5 27.6 20.5 32.6 35.1	29.6 28.3 20.6 32.5 35.1	33.0 30.2 29.0 32.3 35.1	34.5 31.3 29.2 32.3 35.1	37.0 33.3 29.9 32.2 35.0 3	37.8 36.2 30.3 32.2 35.0	18.6 34.9 30.7 32.2 35.0 19.6 19.9 1	40,2 36.4 31.5 32.2 34.9	41.0 17.0 11.9 12.2 34.9	41,0 38.5 32.7 32.2 34.6	41,8 39,3 33,1 32,2 34,8	44.6 40.0 33.6 32.3 34.0	45,6 41,2 34,5 32,4 34,0	46.3 42.3 35.3 32.3 34.6



Appendix C Soil Classification Data

Soil gradation curves along with accompanying sieve data tabulations for each of the soil classification samples taken from the Control Site at Yuma Proving Ground, AZ, are included in the following pages.



PROJECT:

SADARM -- YPG

CONTROL SITE

BORING: WASH BOTTOM SAMPLE: YPG-1 DF: MD0391 .DAT DEPTH: DATE: 03 JAN 91

WC: .00

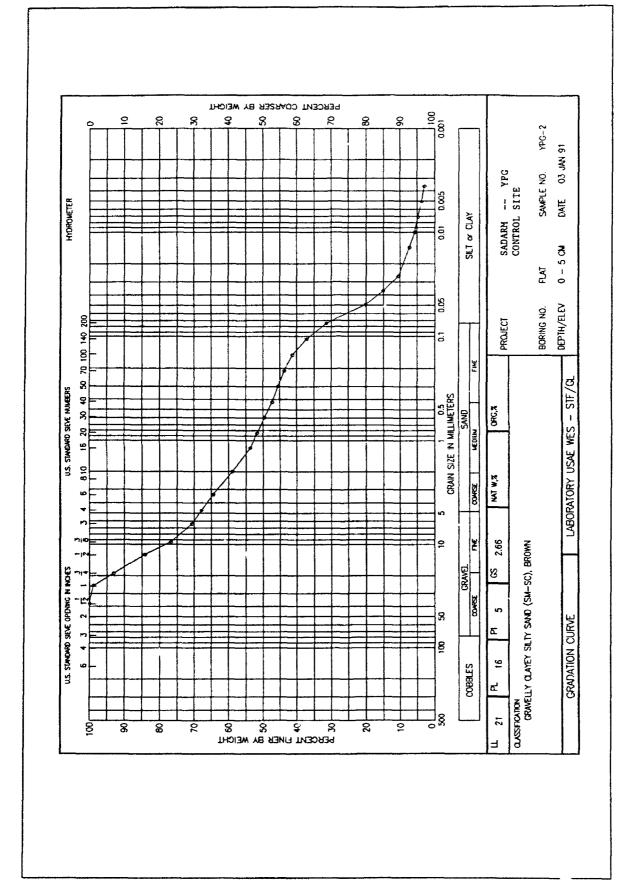
CON-PLASTIC GS: 2.59
CLASSIFICATION: 108
GRAVELLY COM-GRAVELLY SAND (SW), BROWN

TOTAL WEIGHT OF SAMPLE: 2343.0 gms. 'ARTIAL WEIGHT AFTER SPLIT: 61.2 gms.

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
gn.	or NUMBER	mm	FINER	PERCENTS
.0	1 in	25.000	100.0	.0
67.0	3/4 in	19.100	97.1	2.9
178.8	1/2 in	12.500	89.5	10.5
228.6	3/8 in	9.500	79.8	20.2
401.3	No 3	6.350	62.6	37.4
273.7	No 4	4.750	50.9	49.1
319.5	No 6	3.350	37.3	62.7
346.0	No 10	2.000	22.5	77.5
23.1	No 16	1.180	14.0	86.0
33.2	No 20	.850	10.3	89.7
42.1	No 30	.600	7.0	93.0
48.8	No 40	.425	4.6	95.4
51.3	No 50	.300	3.6	96.4
52.8	No 70	.212	3.1	96.9
53.9	No 100	.150	2.7	97.3
55.1	No 140	.106	2.2	97.8
56.3	No 200	.075	1.8	98.2
YDROMETER:				
RDGS	TEMP			
1.3	22.5	.0577	. 8	99.2
1.0	22.5	.0409	. 6	99.4
.8	22.5	.0290	.5	99.5
. 8	22.5	.0150	.5	99.5
.3	22.5	.0106	.2	99.8
.2	22.5	.0075	. 1	99.9
.1	22.5	.0053	. 1	99.9
.1	22.5	.0038	.1	99.9

PERCENT GRAVEL = 49.1 49.061
PERCENT SAND = 49.1 49.139
PERCENT FINES = 1.8

D60 = 5.99 D30 = 2.68 D10 = .83 CU = 7.25 CC = 1.45



PROJECT:

SADARM -- YPG

CONTROL SITE

BORING: FLAT

SAMPLE: YPG-2 DF: MD0391 .DAT

DEPTH: 0 - 5 CM

DATE: 03 JAN 91

L: 21 PL: 16 PI: 5 GS: 2.66 WC:

.00

LASSIFICATION: 126

GRAVELLY CLAYEY SILTY SAND (SM-SC), BROWN

TOTAL WEIGHT OF SAMPLE: 3051.0 gms. ARTIAL WEIGHT AFTER SPLIT: 76.2 gms.

WEIGHTS SIEVE SIZE OPENING PERCENT CUMULATIVE or NUMBER PERCENTS FINER gm. mm .0 29.5 1.5 in 37.500 100.0 .0 l in 25.000 99.0 1.0 179.3 3/4 in 19.100 93.2 6.8 273.8 1/2 in 12.500 84.2 15.8 225.6 3/8 in 9.500 23.2 76.8 183.8 3 4 6.350 70.8 29.2 No 85.8 4.750 No 32.0 68.0 106.4 No 6 3.350 64.5 35.5 169.1 No 10 2.000 58.9 41.1 6.6 No 16 1.180 53.8 46.2 9.3 No 20 .850 51.7 48.3 12.1 50.4 No 30 .600 49.6 15.1 No 40 47.2 52.8 .425 17.3 No 50 .300 45.5 54.5 19.7 No 70 .212 43.7 56.3 22.8 No 100 .150 41.3 58.7 28.1 No 140 .106 37.2 62.8 35.4 No 200 68.5 .075 31.5 YDROMETER: RDGS TEMP 16.3 22.5 .0497 20.2 79.8 12.1 22.5 .0366 15.0 85.0 8.6 .0267 22.5 10.7 89.3 5.9 .0141 7.3 92.7 22.5 4.7 .0100 5.7 94.3 22.0 3.9 95.2 22.5 .0071 4.8

.0051

.0036

3.8

3.0

96.2

97.0

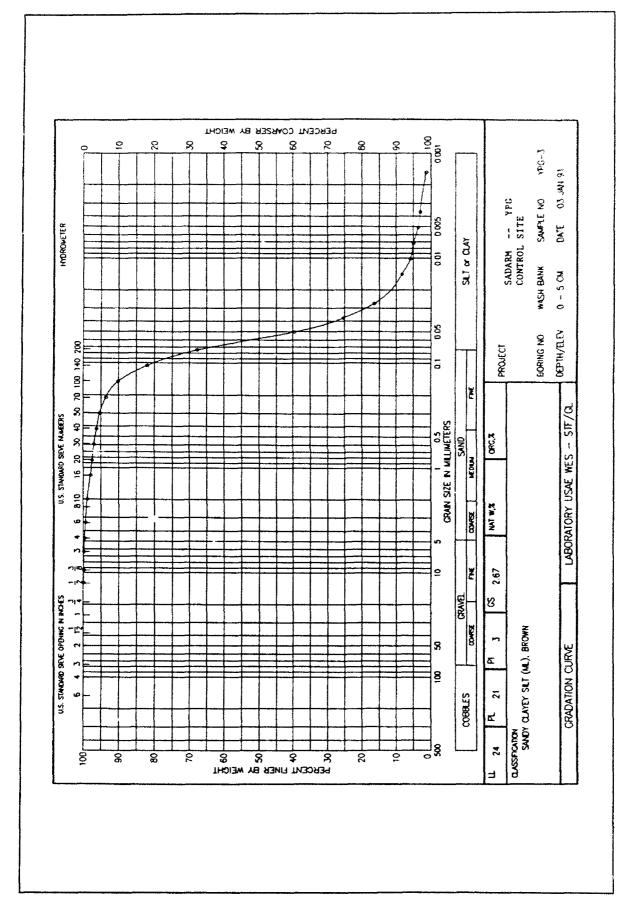
PERCENT GRAVEL = 32.0 PERCENT SAND = 36.4 PERCENT FINES = 31.5

22.5

22.5

3.1

2.4



PROJECT:

SADARM -- YPG

CONTROL SITE

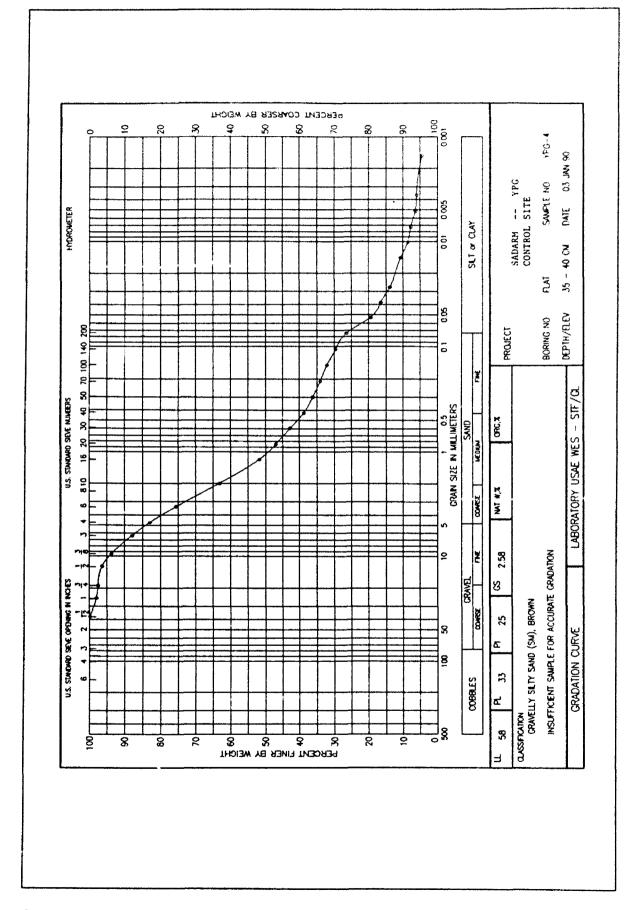
BORING: WASH BANK SAMPLE: YPG-3 DF: MD0391A .DAT DEPTH: 0 - 5 CM DATE: 03 JAN 91

LL: 24 PL: 21 PI: 3 GS: 2.67 CLASSIFICATION: 144 SANDY CLAYEY SILT (ML), BROWN WC: .00

TOTAL WEIGHT OF SAMPLE: 2425.0 gms. PARTIAL WEIGHT AFTER SPLIT: 56.7 gms.

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
on.	or NUMBER	mm	FINER	PERCENTS
.0	1/2 in	12.500	100.0	.0
1.4	3/8 in	9.500	99.9	.1
2.4	NO 3	6.350	99.8	.2
3.9	No 4	4.750	99.7	.3
5.2	No 6	3.350	99.5	.5
13.1	No 10	2.000	98.9	1.1
1911	70 10	2.000	20.9	***
.5	No 16	1.180	98.1	1.9
.8	No 20	.850	97.5	2.5
1.1	No 30	.600	97.0	3.0
1.5	No 40	.425	96.3	3.7
2.0	No 50	.300	95.4	4.6
3.0	No 70	.212	93.7	6.3
5.0	No 100	.150	90.2	9.8
9.7	No 140	.106	82.0	18.0
17.8	No 200	,075	67.9	32.1
HYDROMETER:				
RDGS	TEMP			
14.2	22.5	.0506	39.6	60.4
9.1	22.5	.0374	25.4	74.6
5.9	22.5	.0272	16.5	83.5
3.0	22.5	.0144	8.4	91.€
2.2	22.0	.0102	5.9	94.1
1.8	22.5	.0072	5.0	95.0
1.3	22.5	.0051	3.6	96.4
1.1	22.5	.0036	3.1	96.9
.9	20.5	.0015	1.4	98.6

PERCENT GRAVEL = .3 PERCENT SAND = 31.8 PERCENT FINES = 67.9



PROJECT:

SADARM -- YPG

CONTROL SITE

BORING: FLAT SAMPLE: YPG-4 DF: MD0391 .DAT DEPTH: 35 - 40 CM DATE: 03 JAN 90

PL: 33 PI: 25 GS: 2.58 WC: .00

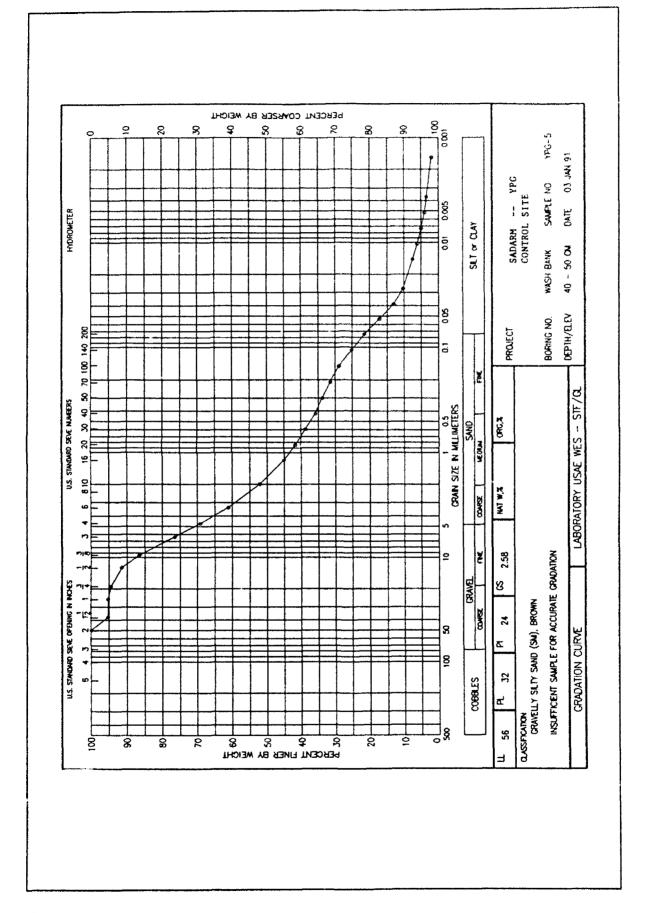
LASSIFICATION: 162

GRAVELLY SILTY SAND (SM), BROWN

TOTAL WEIGHT OF SAMPLE: 2396.0 gms. 'ARTIAL WEIGHT AFTER SPLIT: 68.0 gms. 'NSUFFICIENT SAMPLE FOR ACCURATE GRADATION

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
gna.	or NUMBER	mm	FINER	PERCENTS
.0	1.5 in	37.500	100.0	.0
47.2	1 in	25.000	98.0	2.0
10.9	3/4 in	19.100	97.6	2.4
27.5	1/2 in	12.500	96.4	3.6
64.0	3/8 in	9.500	93.8	6.2
138.7	No 3	6.350	88.0	12.0
117.6	No 4	4.750	83.1	16.9
178.6	No 6	3.350	75.6	24.4
296.3	No 10	2.000	63.2	36.8
12.3	No 16	1.180	51.8	48.2
17.4	No 20	.850	47.1	52.9
22.0	No 30	.600	42.8	57.2
26.3	No 40	.425	38.8	61.2
29.0	No 50	.300	36.3	63.7
31.3	No 70	.212	34.1	65.9
33.3	No 100	.150	32.3	67.7
36.1	No 140	.106	29.7	70.3
39.5	No 200	.075	26.5	73.5
YDROMETER:				
RDGS	TEMP			
13.0	21.5	.0532	19.4	80.6
11.1	21.5	.0383	16.6	83.4
9.4	21.5	.0275	14.0	86.0
7.3	21.5	.0144	10.8	89.2
5.9	21.5	.0103	8.7	91.3
5.3	21.5	.0073	7.7	92.3
4.3	22.0	.0052	6.4	93.6
4.1	22.0	.0037	6.1	93.9
3.2	21.5	.0015	4.6	95.4

PERCENT GRAVEL = 16.9 PERCENT SAND = 56.6 PERCENT FINES = 26.5



PROJECT:

SADARM -- YPG

CONTROL SITE

BORING: WASH BANK SAMPLE: YPG-5 DF: MD0391A .DAT

DEPTH: 40 - 50 CM DATE: 03 JAN 91

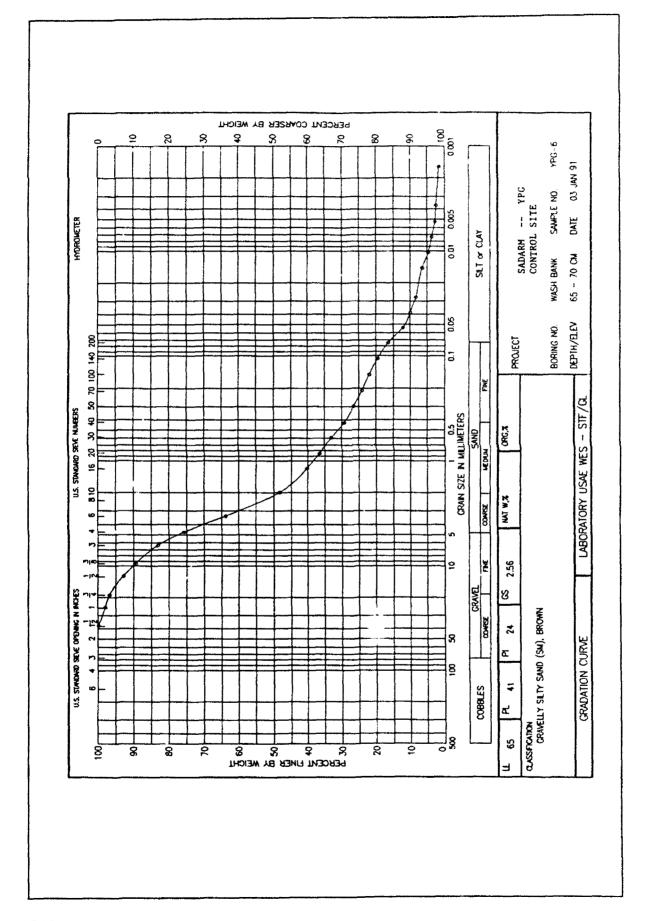
LL: 56 PL: 32 PI: 24 GS: 2.58 WC: .00 CLASSIFICATION: 180

GRAVELLY SILTY SAND (SM), BROWN

TOTAL WEIGHT OF SAMPLE: 2032.0 gms. PARTIAL WEIGHT AFTER SPLIT: 54.3 gms. INSUFFICIENT SAMPLE FOR ACCURATE GRADATION

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
gm.	or NUMBER	mm	FINER	PERCENTS
.0	2 in	50.000	100.0	.0
94.0	1.5 in	37.500	95.4	4.6
.0	1 in	25.000	95.4	4.6
16.5	3/4 in	19.100	94.6	5.4
61.0	1/2 in	12.500	91.6	8.4
99.7	3/8 in	9.500	86.7	13.3
205.7	No 3	6.350	76.5	23.5
148.0	No 4	4.750	69.2	30.8
163.8	No 6	3.350	61.2	38.8
183.6	No 10	2.000	52.2	47.8
7.3	No 16	1.180	45.1	54.9
10.9	No 20	.850	41.7	58.3
13.9	No 30	.600	38.8	61.2
16.9	No 40	.425	35.9	64.1
19.0	No 50	.300	33.9	66.1
21.4	No 70	.212	31.6	68.4
24.2	No 100	.150	28.9	71.1
28.1	No 140	.106	25.2	74.8
31.9	No 200	.075	21.5	78.5
HYDROMETER:				
RDGS	TEMP			
11.0	22.5	.0535	17.3	82.7
8.4	22.5	.0387	13.2	86.8
6.6	22.5	.0278	10.4	89.6
4.8	22.5	.0146	7.5	92.5
3.9	22.5	.0104	6.1	93.9
3.2	22.5	.0074	5.0	95.0
2.6	22.5	.0052	4.1	95.9
2.1	23.0	.0037	3.5	96.5
1.7	20.5	.0016	2.0	98.0

PERCENT GRAVEL = 30.8 PERCENT SAND = 47.7 PERCENT FINES = 21.5



PROJECT:

SADARM -- YPG CONTROL SITE

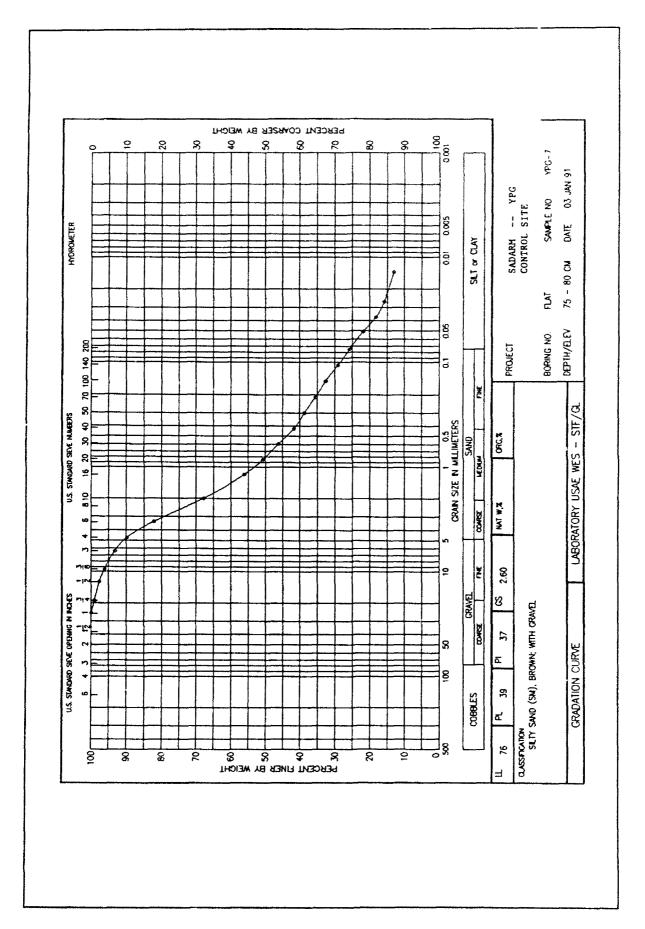
BORING: WASH BANK SAMPLE: YPG-6 DF: MD0391 .DAT DEPTH: 65 - 70 CM DATE: 03 JAN 91 BORING: WASH BANK

.L: 65 PL: 41 PI: 24 GS: 2.56 WC: .00 CLASSIFICATION: 198 GRAVELLY SILTY SAND (SM), BROWN

TOTAL WEIGHT OF SAMPLE: 2539.0 gms. 'ARTIAL WEIGHT AFTER SPLIT: 71.9 gms.

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
cm.	or NUMBER	mm	FINER	PERCENTS
.0	1.5 in	37.500	100.0	.0
50.3	1 in	25.000	98.0	2.0
30.3	3/4 in	19.100	96.8	3.2
98.1	1/2 in	12.500	93.0	7.0
89.0	3/8 in	9.500	89.5	10.5
157.9	No 3	6.350	83.2	
190.5	No 4	4.750	75.7	16.8
301.1	No 6	3.350	63.9	24.3
391.8	No 10	2.000	48.4	36.1
	10	2.000	40.4	51.6
12.0	No 16	1.180	40.4	59.6
17.5	No 20	.850	36.7	63.3
22.8	No 30	.600	33.1	65.9
28.4	No 40	.425	29.3	
32.5	No 50	.300	26.5	70.7
36.2	No 70	.212	24.1	73.5
39.2	No 100	.150		75.9
43.0	No 140	.106	22.0	78.0
47.3	No 200		19.5	80.5
YDROMETER:	NO 200	.075	16.6	83.4
RDGS	TEMP			
11.0	22.5	0500		
9.1		.0539	12.2	87.8
7.6	22.5	.0387	10.1	6.63
5.9	22.5	.0277	8.4	91.6
4.3	22.5	.0145	6.5	93.5
	22.5	.0104	4.8	95.2
3.3	22.5	.0074	3.6	96.4
2.5	22.5	.0053	2.8	97.2
2.1	23.0	.0037	2.4	97.6
1.8	20.5	.0016	1.5	98.5

PERCENT GRAVEL = 24.3 PERCENT SAND = 59.2 PERCENT FINES = 16.6



PROJECT: SADARM -- YPG

CONTROL SITE

BORING: FLAT SAMPLE: YPG-7 DF: MD0391 .DAT DEPTH: 75 - 80 CM DATE: 03 JAN 91 BORING: FLAT

.L: 76 PL: 39 PI: 37 GS: 2.60 WC: .00 LASSIFICATION: 216 SILTY SAND (SM), BROWN; WITH GRAVEL

TOTAL WEIGHT OF SAMPLE: 4194.0 gms. ARTIAL WEIGHT AFTER SPLIT: 75.7 gms.

WEIGHTS	SIEVE SIZE	OPENING	PERCENT	CUMULATIVE
gm.	or NUMBER	inm	FINER	PERCENTS
.0	1 in	25.000	100.0	.0
36.1	3/4 in	19.100	99.1	.9
60.7	1/2 in	12.500	97.7	2.3
62.0	3/8 in	9.500	96.2	3.8
121.6	No 3	6.350	93.3	6.7
146.3	No 4	4.750	89.8	10.2
318.4	No 6	3.350	82.2	17.8
605.1	No 10	2.000	67.8	32.2
		21440	07.0	32.2
12.9	No 16	1.180	56.3	43.7
19.1	No 20	.850	50.7	49.3
24.1	No 30	-600	46.2	53.8
29.1	No 40	.425	41.7	58.3
32.5	No 50	.300	38.7	61.3
36.0	No 70	.212	35.6	64.4
39.2	No 100	.150	32.7	67.3
43.2	No 140	.106	29.1	70.9
46.9	No 200	.075	25.8	74.2
YDROMETER:		,	23.0	74.2
RDGS	TEMP			
15.1	22.0	.0512	21.8	78.2
12.5	22.5	.0371	18.2	81.8
10.9	22.5	.0266	15.9	84.1
9.0	22.5	.0140	13.3	
		.0140	4.9.5	86.9

PERCENT GRAVEL = 10.2 PERCENT SAND = 64.0 PERCENT FINES = 25.8

Appendix D Photographs of Dominant Plant Species

This appendix contains photographs of most of the dominant plant species found at the Sense and Destroy Armor test area and the Control Site. In three cases, for the plants designated, CEMI, LATR, and OLTE, photos taken before and after local heavy rains show how much vegetation appearance can change as a result of different recent weather histories. These are not before-and-after photographs of the same plants; however, the change in leaf density is typical.

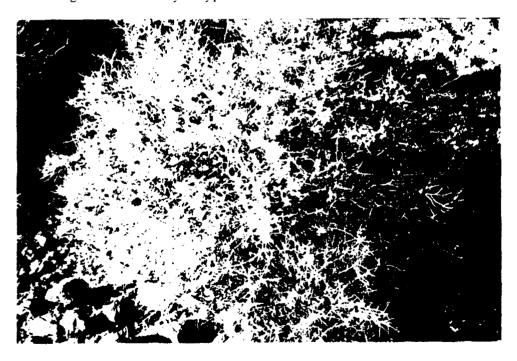


Figure D1. Ambrosia dumosa (white bur sage), AMDU



a. Full view



b. Close-up view

Figure D2. Cercidium microphyllum (yellow palo verde), CEMI, prerain



a. Full view



b. Close-up view

Figure D3 Cercidium microphyllum (yellow palo verde), CEMI, postrain



a. Full view

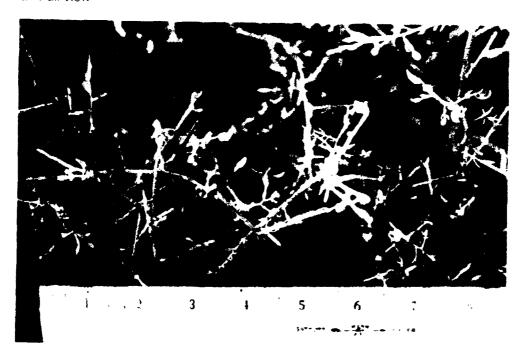


b. Close-up view

Figure D4. Encelia farinosa (brittlebush), ENFA



a. Full view



b. Close-up view

Figure D5. Krameria paravifolia (white ratany), KRPA



a. Full view

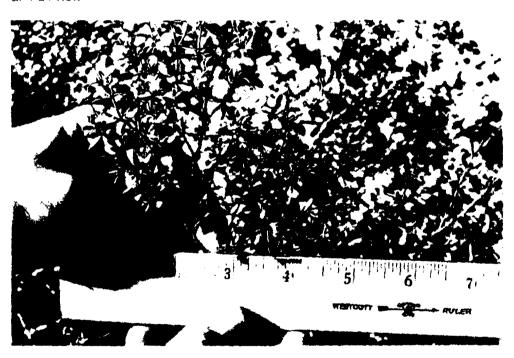


b. Close-up view

Figure D6. Larrea tridentata (creosote bush), LATR, prerain



a. Full view



b. Close-up view

Figure D7. Larrea tridentata (creosote bush), LATR, postrain



a. Full view



b. Close-up view

Figure D8. Lycium sp. (wolfberry), LY--



a. Full view



b. Close-up view

Figure D9. Olyneya tesota (desert ironwood), OLTE, prerain



a. Full view



b. Close-up view

Figure D10. Olyneya tesota (desert ironwood), OLTE, postrain

Appendix E Photographs Depicting Thermal Infrared Image Views

The following photographs taken from the observation tower at the Control Site near the Sense and Destroy Armor test area, Yuma Proving Ground, AZ, are intended to give the general impression of how the thermal infrared imaging cameras were pointed for each recording. The number of degrees shown on each figure represents the depression angle of the cameras.



Figure E1. Scene 1, west wash, 7.5 deg



Figure E2. Scene 2, 14.5 deg



Figure E3. Scene 3, 22.5 deg



Figure E4. Scene 4, 17.5 deg



Figure E5. Scene 5, 20.5 deg



Figure E6. Scene 6, 32 5 deg



Figure E7. Scene 7, 14 deg



Figure E8 Scene 8, 10 deg



Figure E9 Scene 9, 10 deg

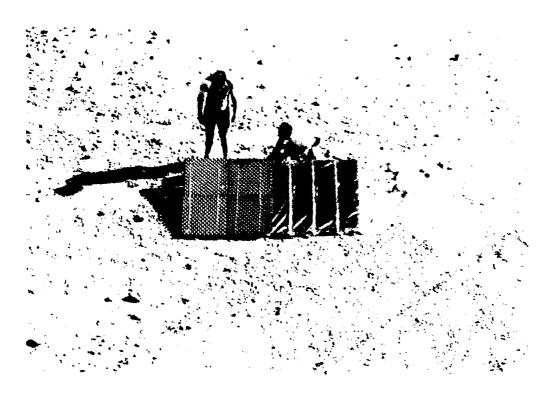


Figure E10 Scene 10, NRL calibration panels, 34 deg

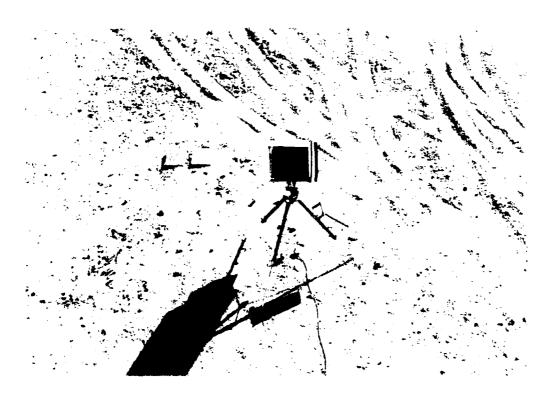


Figure E11. Scene 11, infrared calibration devices, 30 deg

Appendix F Spot Measurement Thermal Infrared Data

The following photographs show the terrain features toward which the staring radiometers were pointed during spot measurements of thermal infrared signatures collected at Yuma Proving Ground, AZ, in September 1990. Also included in this Appendix is a tabulation of the 15-min averages of the apparent temperatures measured by each of the radiometers.

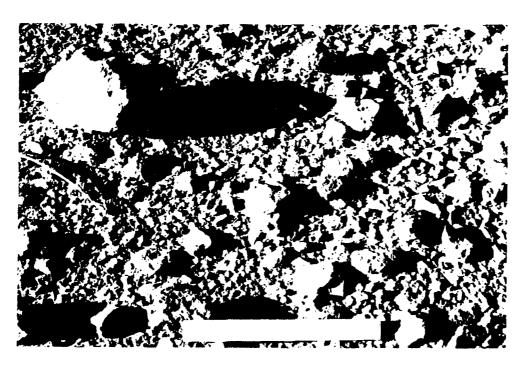


Figure F1. Radiometer 1, desert pavement

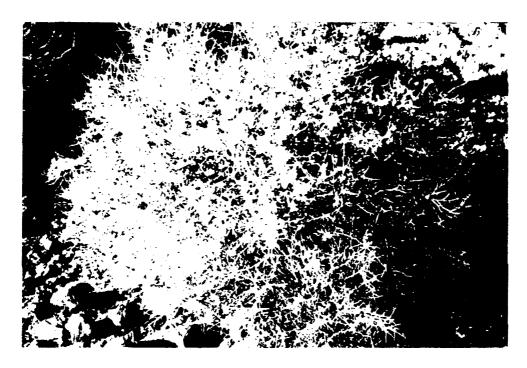


Figure F2. Radiometer 2, vegetation species AMDU

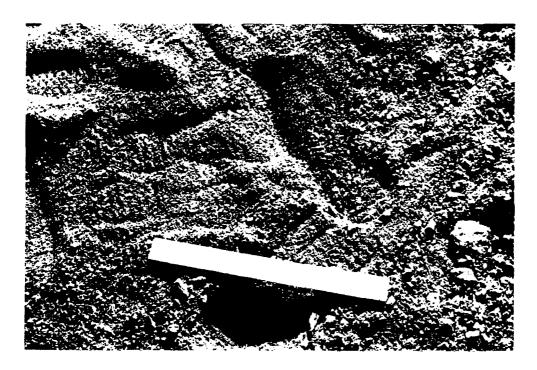


Figure F3. Radiometer 3, gravelly sand in wash bottom

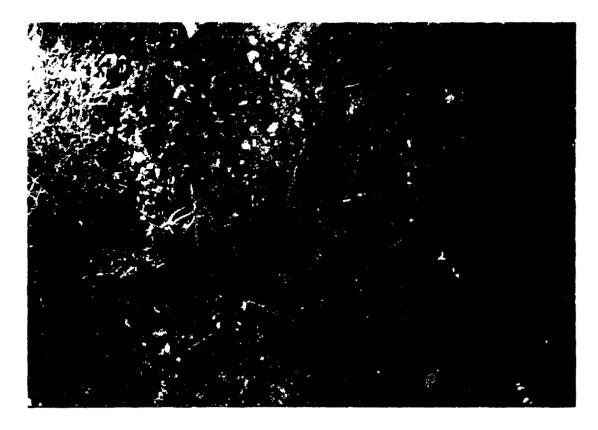


Figure F5. Radiometer 5. north-facing bank of wash



Figure F4. Radiometer 4, shaded soil on north bank of wash

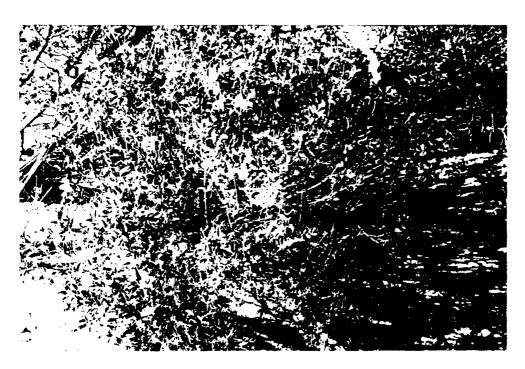


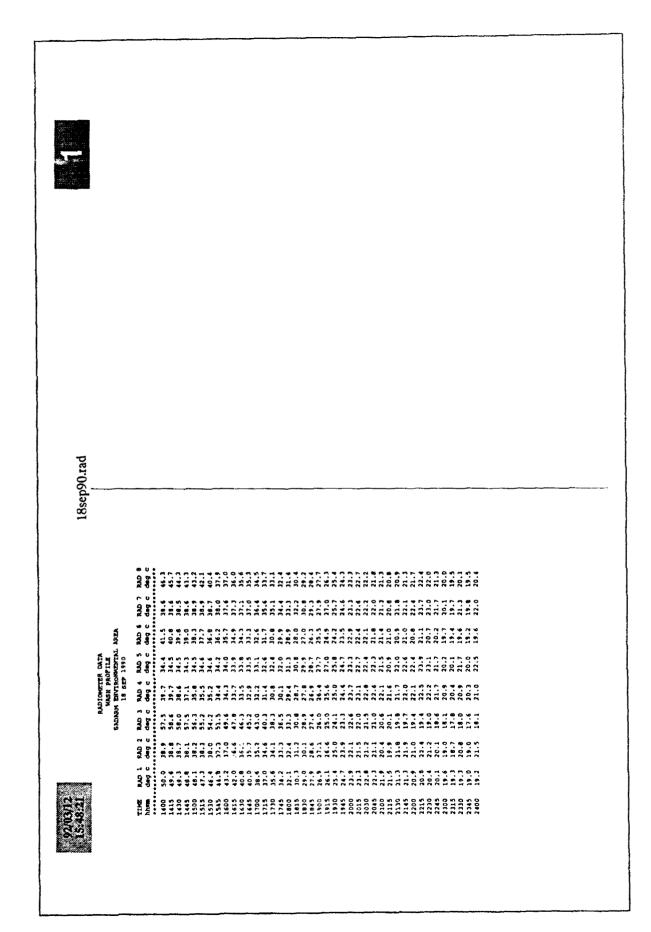
Figure F6. Radiometer 6, vegetation species ENFA

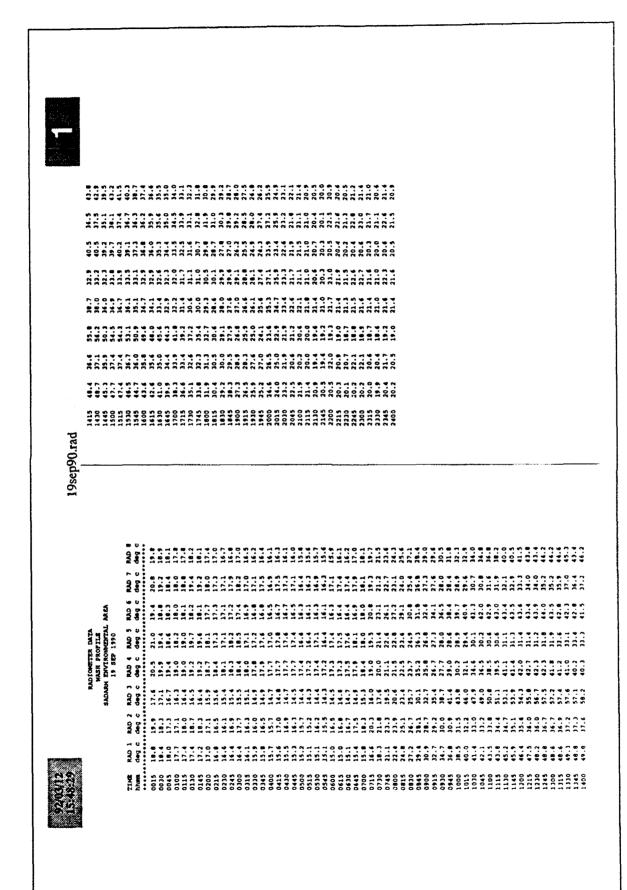


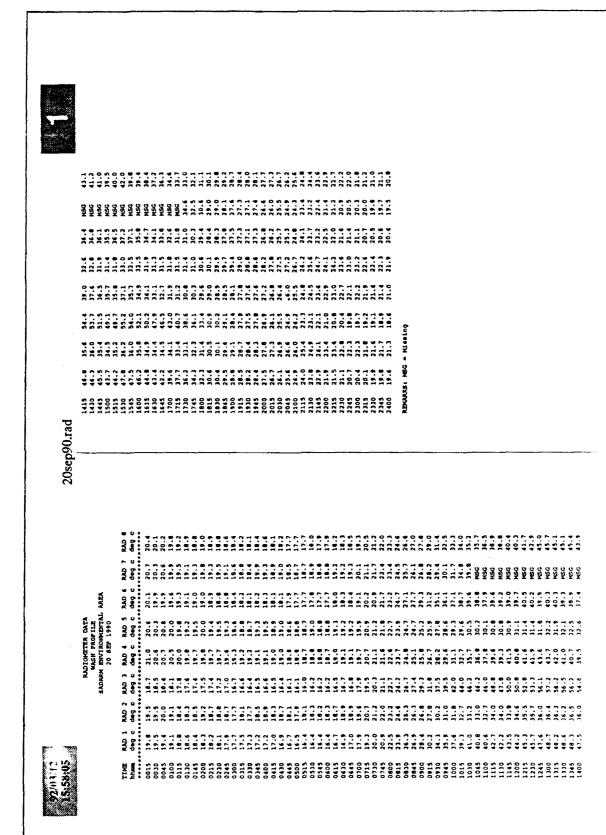
Figure F7. Radiometer 7, bush at base of tree, looking east, later pointed toward silty bank soil

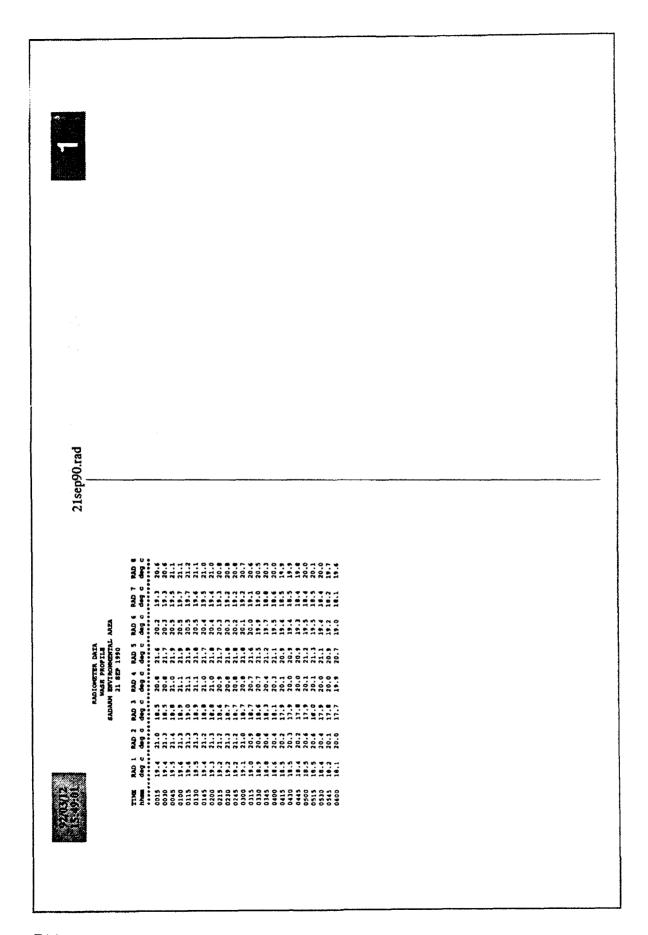


Figure F8. Radiometer 8, south-facing deadwood









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This report provides an outline of the test site environmental characterization support completed at the U.S. Army Yuma Proving Ground for the Sense and Destroy Armor (SADARM) Captive Flight Test conducted during September 1990. Personnel from two U.S. Army Corps of Engineers laboratories, the U.S. Army Engineer Waterways Experiment Station and the Cold Regions Research and Engineering Laboratory, collected data during a 2-week period to both qualitatively and quantitatively define the ambient desert terrain and meteorological conditions that provide the background signatures for the SADARM system. Information collected included that necessary to assess the boundary layer radiation exchange process, the characteristics of the ground surface, and the characteristics of the vegetation present in this arid environment. A fixed tower was erected adjacent to a representative patch of desert terrain to provide a platform from which both static and dynamic processes could be observed. Sensors used to view the representative environmental plot included thermal imaging systems that operated in both the 3- to 5-\mu m and 8- to 12-\mu m

wavelength bands, an active millimeter wave system that swept a frequency band of 33.0 to 33.5 GHz, and

two scanning radiometers operated by the Naval Research Laboratory.

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